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KARA NO 2 NORTH

MINERAL RESOURCE ESTIMATE

NW TASMANIA

Prepared for: Forward Mining Limited

Tim Callaghan, August 2011

MAP CONVENTIONS

Coordinates in this report and in digital data associated with this report are recorded as GDA94 Zone 55.

RL's in this report are MSL.

Cross sections are drawn looking north.

EXECUTIVE SUMMARY

The Kara District magnetite-tin-tungsten skarns are hosted in calcareous sediments of the Ordovician Gordon Group. Calc-silicate and magnetite skarn mineralisation has formed through metasomatic replacement of limestone in direct contact with the Housetop Granite.

There are numerous calc-silicate-magnetite skarns of this style in the district, the two biggest known deposits being the Kara No 1 Skarn currently in production and operated by Tasmanian Mines Ltd, and the Kara No 2 Skarn managed by Forward Mining Ltd. The Kara No 1 and Kara No 2 Skarns are directly analogous in geological setting, morphology and mineralogy.

The Kara No 2 skarn consists of a cluster of four calc-silicate and magnetite skarn deposits occurring as roof pendants on the top of the Housetop Granite, the largest of which is Kara No 2 North, followed by Kara No 2 East, Kara No 2 South and the small Button Grass deposit. All the deposits have been historically explored, mainly for tin and tungsten skarn mineralisation with the majority of the work completed by MacIntyre Mines in the 1980's. The recent (2008-2009) Iron Mountain (IRM) - Red River (RVR) Joint Venture focused their exploration on magnetite skarn mineralisation completing several drilling campaigns.

The IRM-RVR drilling concentrated on the Kara No 2 North skarn with a few exploration drill holes completed on the other three deposits. Drilling density of the Kara No 2 North skarn is sufficient for the estimation of an Inferred Resource according to the JORC code (Table 1).

Table 1. Kara No 2 North Inferred Resource

	MTonnes	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
Oxidised	2.15	42.1	0.10	0.10	11.0	0.04	0.08
Un-oxidised	14.47	36.7	0.08	0.08	16.1	0.03	0.28
Total	**16.62**	**37.4**	**0.08**	**0.08**	**15.4**	**0.03**	**0.25**

The deposit forms a gently south plunging synclinal structure in the roof of the Houstop Granite with a steep western margin and gently shelving eastern margin. Oxidation of the calc-silicate skarn extends to approximately 20-30m depth. Magnetic susceptibility measurements on drill holes suggest magnetite is present in the oxidised magnetite skarn as well as limonite and goethite. Just over 10% of the deposit is oxidized.

The deposit remains open to the south for a limited strike extent and possibly at depth in the south plunging syncline.

The shallow plunging Kara No 2 skarn morphology is amenable to conventional open cut mining.

Recommendations for future work include:

- Infill drilling to 50m spaced sections.
- Geotechnical logging of future drilling campaigns

- Further bulk density measurements on diamond drill core.
- Davis Tube Recoveries and metallurgical testwork on drill core samples
- Initiation of a QA/QC regime in future drilling programs.
- Estimation of Measured and Indicated Mineral Resource
- Pit optimization studies and reserve definition.
- Resource extension and exploration drilling.

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1 INTRODUCTION

The Blythe River Iron Project (BRIP) consists of a number of small to medium size magnetite skarn deposits located in NW Tasmania, approximately 30km south of Burnie (Figure 1 and 2). The project is covered by six Exploration License's held by either Iron Mountain Mining Ltd (IRM) or Red River Resources Ltd (RVR) and managed by Forward Mining Limited (FML).

Table 2. Blythe River Project Tenure

EL	**Held By**	**Size**	**Expiry**	**Comments**
EL6/2005	IRM	22km^2	9/2011	Apply for Extension
EL15/2006	IRM	30km^2	6/2011	Apply for Extension
EL25/2009	RVR	33km^2	5/2015	4 years remaining
EL35/2006	RVR	89km^2	2/2012	Expires early 2012
EL18/2007	RVR	103km^2	7/2012	Expires mid 2012
EL53/2007	IRM	47km^2	12/2012	2 years remaining

Four of the deposits, Kara No 2 North, Kara No 2 East, Kara No 2 South and Button Grass are located in a cluster on the boundary of EL18/2007 and EL53/2007. Tasmanian Mines have a small ML located within the vicinity of these deposits that has historically produced magnetite from a small open cut (Figure 1 - 3). The Kara No 2 skarns form the initial focus of operations in the Blythe River area for FML.

The Kara No1 Skarn located 4-5km to the east is operated by Tasmanian Mines Ltd. Their operations comprise an open cut and mill producing 2-3ktpa of magnetite concentrate used mainly for coal washing and by product Scheelite. Some magnetite is sold to Grange Resources to supplement magnetite iron ore production.

Tim Callaghan Resource and Exploration Geology (REG) was engaged by FML to prepare a mineral resource estimate for the Kara No 2 North deposit.

Mineral resource estimates in this report have been classified and reported in accordance with the Australasian CODE for Reporting of Exploration Results, Mineral Resources and Ore Reserves, 2004 edition (the "JORC" code).

1.1 SCOPE OF WORK

REG propose to carry out the following work on the Kara No 2 North deposit:

- Locate, load and validate exploration data into ACCESS database
- Provide geological interpretation of the deposits
- Prepare three dimensional solid models of geological elements required for resource estimation
- Create a digital terrain model of the Kara No 2 area
- Undertake statistical and geostatistical investigations
- Prepare a block model of the Kara No 2 North deposit
- Estimate total Fe, WO_3, SnO_2, CaO, P_2O_5 and SO_3 into the model.
- Validate the model

- Report the mineral resource in accordance with the JORC Code

1.2 DATA PROVIDED

Data used for this estimate includes:

- Drill logs and assay data
- Ground magnetic data
- Aeromagnetic image
- MRT 1:250 000 mapping
- Historic exploration company 1:10 000 mapping
- Mineral Resources Tasmania 1:25 000 mapping

No documentation of QA/QC or data validation was provided or cited with the IRM-RVR drilling programs. Several errors were identified in the drilling data and corrected before geological modeling commenced.

Errors corrected include

- Assay interval overlaps
- Geology interval overlaps
- Magnetic susceptibility overlaps
- Incorrect end of hole depths

Data provided with this report includes:

- Access database
- Digital terrain model of the Kara No 2 district
- Solid Models of major Geological Elements (Surpac)
- Solid Models of Mineralisation Domains (Surpac)
- Block modeled Resource Estimate (Surpac)
- 1:1000 scale cross sections
- Mineral Resource Estimate Report (pdf)
- JORC Consent Form

2 GEOLOGY

2.1 REGIONAL GEOLOGY

The Blythe River Iron Project is located on the western margin of the Dial Range Trough and is underlain by lithologies of the Late Proterozoic Oonah Formation, Owen Group Siliciclastics, Gordon Group Limestone, Devonian Granites and Tertiary Basalt (Figure 1). The Dial Trough is a structurally interesting basin that includes a possible Northern Extension of the Hellyer Fault, and significant basin bounding faults on the western and eastern sides. The Devonian post orogenic Housetop Granite dominates the geology to the south of the project area and is considered to underlie much of the southern dial trough. The Dial Trough has been poorly mapped and stratigraphic correlations are uncertain for many units.

Oonah Formation

The oldest rocks in the district are the Proterozoic Oonah formation, consisting of poly-deformed quartzwacke, siltstone and pelite with lesser dolerite intrusives. These are overlain by a sequence of pelite-carbonate with minor mafic volcanics and conglomerate. This association is host to replacement deposits at Mt Bischoff and near Zeehan and consequently represents a potential host for similar styles of skarn mineralisation.

Mt Read Volcanics

Mt Read Volcanic associations have been correlated with the felsic volcaniclastics of the Western Volcano-sedimentary sequence and the Tyndall Group quartz-feldspar phyric volcaniclastics.

Owen Group

The Late Cambrian to Ordovician Owen Group overlies the Mt Read Volcanics and is comprised dominantly of siliciclastic conglomerate and sandstone. Locally volcanic derived conglomerates are associated with basal members. The Moina Sandstone, comprised of coarse to fine siliciclastic sandstone with minor intercalated conglomerate is the uppermost siliciclastic unit of the Owen Group and has a gradational contact with the overlying Gordon Group.

Gordon Group Limestone

Conformably overlying the Owen Group is the Gordon Group limestone and dolomite sequence which is the host of the Kara district magnetite skarns. The stratigraphic thickness of the limestone is regionally variable ranging between 50-1000m.

Housetop Granite

The Housetop granite outcrops in much of the Blythe River Prospect and is believed to extend below much of the area (Leaman, 1993). Leaman concludes that the Housetop granite is anomalously dense and highly magnetic, which may explain the abundance of iron metasomatism in the district. The granite is responsible for massive Magnetite-Sn-WO_3 mineralisation of the Kara District. The association of Tasmanian Devonian granites with Magnetite, Sn-WO_3, Pb-Zn-Ag and Au mineralisation is well documented.

Tertiary Basalt

Basaltic flows are widespread throughout the Blythe River Iron Project area, flooding Tertiary palaeo-topographic lows. The basalts vary widely in thickness and frequently have a high magnetic susceptibility creating difficulties for magnetite exploration below basaltic cover. Recent resource and exploration drilling at the Kara Mine indicates that the magnetite skarn extends below basalt cover.

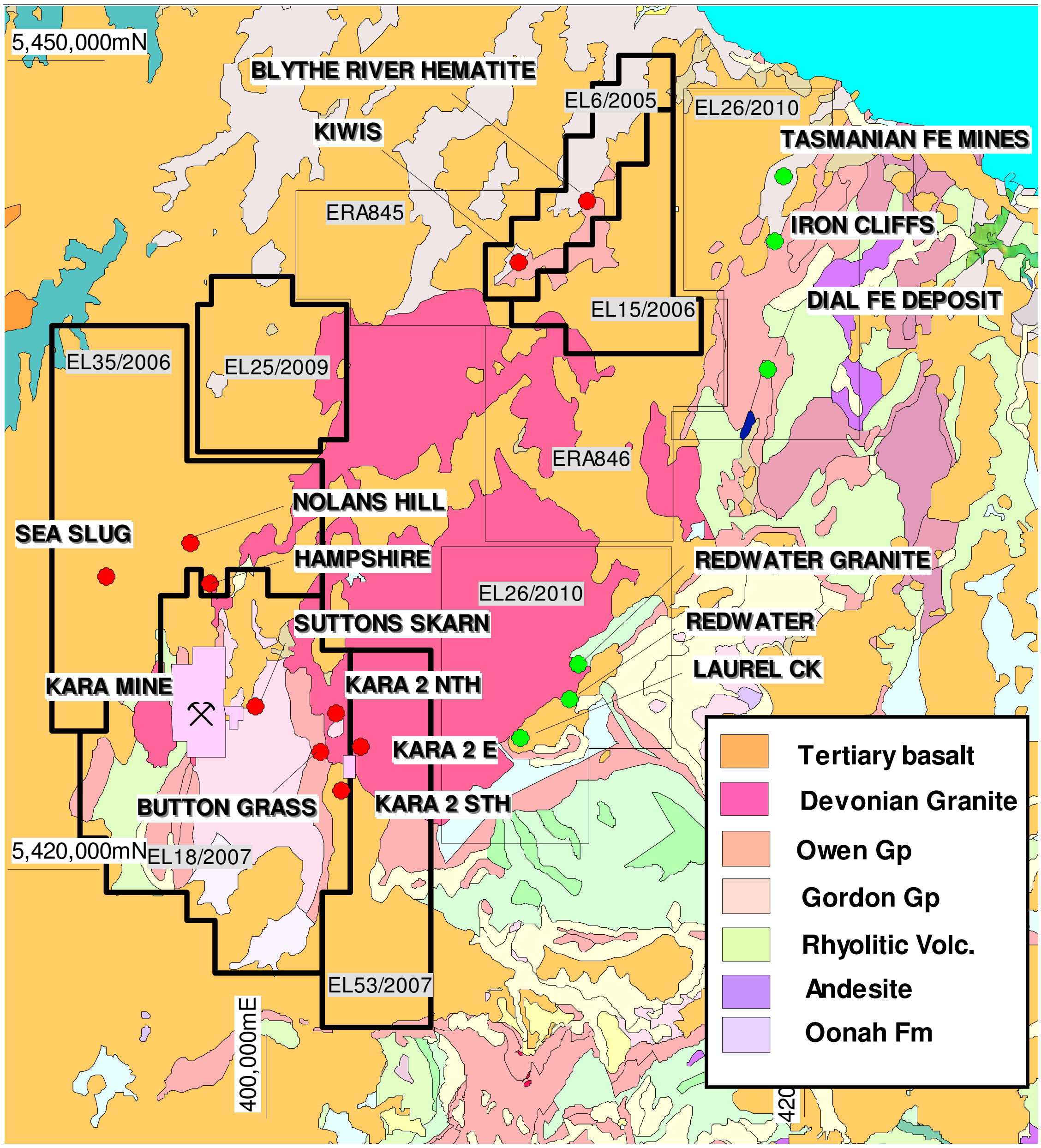

Figure 1. Blythe River Project location, Fe Prospects and MRT 250k Geology. Red dots are Blythe Project Fe prospects, green dots are other regional Fe Prospects.

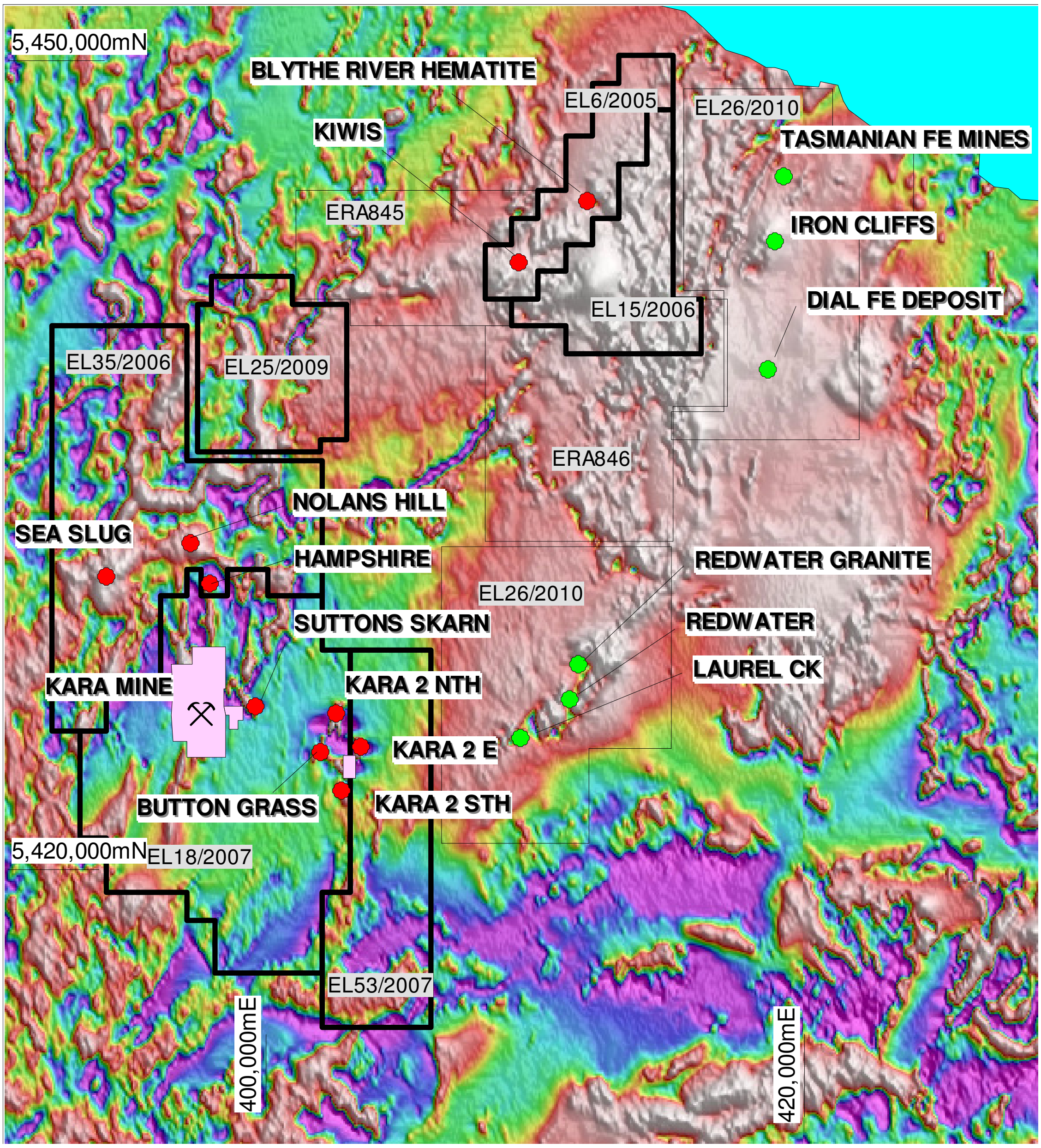

Figure 2. Blythe Project tenements, TMI and prospect locations. Red dots are Blythe Project Fe prospects, green dots are other regional Fe Prospects.

2.2 LOCAL GEOLOGY.

The Kara No 2 Skarns are hosted in folded roof pendants of Gordon Limestone and Moina Sandstone inliers within the Housetop Granite batholith. Magnetite skarns obviously have a very high magnetic susceptibility and form prominent aeromagnetic highs (Figure 3).

Geological mapping of the area is sparse with the best map available being a 1:10 000 map completed by MacIntyre Mines in 1982 (Whitehead, 1982), supported by 1:25 000 mapping by Mineral Resources Tasmania.

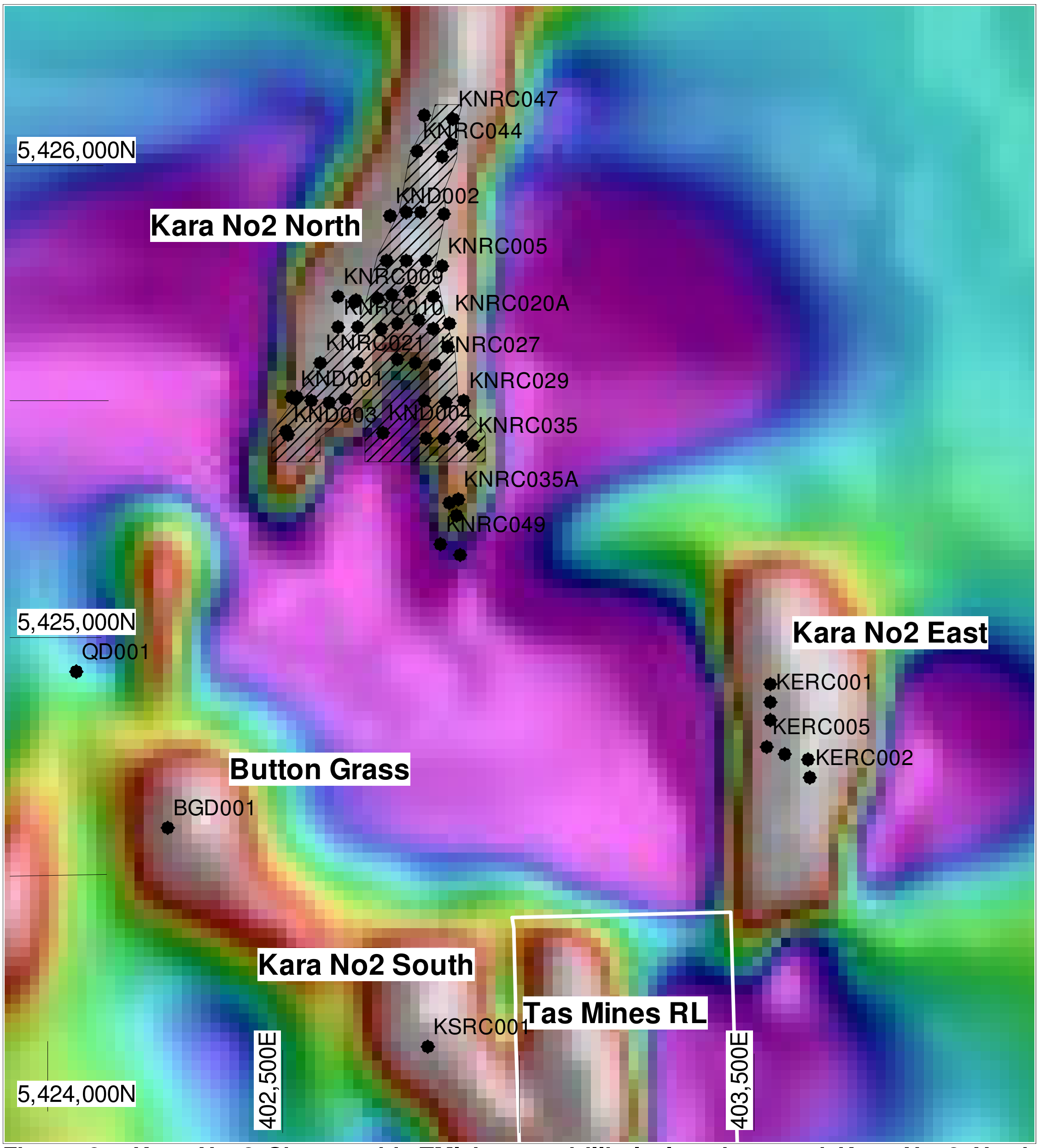

Figure 3. Kara No 2 Skarns with TMI image, drillhole locations and Kara No 2 North resource outline.

Skarn mineralogy is complex, however Zaw (2000) has identified a minimum of 4 stages of skarn formation at the Kara No1 deposit. The geology and morphology of the Kara No 2 skarns are essentially identical in mineralogy and morphology to those of the Tasmania Mines operated Kara No1 skarns.

Several major skarn facies are highlighted in drill core and rock chips including:

- Diopside skarn (SKPX)
- Garnet skarn (SKGT)
- Magnetite-diopside skarn (SKMG)
- Magnetite-amphibole-epidote skarn (SKMG)
- Calc-silicate skarn (calcite-epidote-chlorite and amphibole) (SKCS)
- Marble (LMST)

The magnetite-diopside and magnetite-amphibole-epidote skarn assemblages form the basis of this resource estimate. Magnetite occurs as coarse disseminated euhedral crystals, veins and massive aggregates within a diopside or amphibole rich matrix. Mineralogical boundaries of skarn facies vary from sharp to gradational. Magnetite contents are variable but where present generally occur as coarse magnetite.

Zaw (2000) suggests WO_3 and SnO_2 mineralisation is most commonly associated with the more hydrous magnetite-amphibole-epidote skarn phase.

The Kara No 2 Skarns are located in relatively flat terrain dominated by low re-growth eucalypt forest on crown land managed by Forestry Tasmania. Access roads are well formed unsealed forestry roads.

The best drilled and largest deposit of the Kara No 2 Skarns is the Kara No 2 North Skarn. This is the only deposit of the Kara No 2 Skarns currently drilled sufficiently to allow estimation of mineral resources.

The deposit consists of a north-south striking, gently south plunging asymmetric syncline of Ordovician Gordon Group limestone and lesser Moina Sandstone lying directly on top of the Housetop granite. The western limb is vertical and the eastern limb is gently shelving (Figure 4).

The deposit occurs over a strike length of 800m and is approximately 100m wide at the shallow northern end, grading to in excess of 500m width as it plunges south. Mineralisation outcrops in the northern end and on the syncline limbs and extends to over 120m depth at the south end. The deposit remains open to the south for a limited distance as suggested by aeromagnetic images, but is closed off at approximately 5,425,100N (Figure 5). There is potential to add significantly more tonnes at the deeper southern end of the deposit.

Thick (10-60m) magnetite skarn mineralisation has been intersected in many drill holes, with a relatively consistent lens of mineralisation occurring directly over the granite, forming a shallow south plunging synform. Other less continuous lenses of magnetite skarn mineralisation are present but have not been modeled in this resource estimate due to their limited extent and gradational nature. These satellite lenses of mineralisation may possibly be recoverable during open pit mining operations.

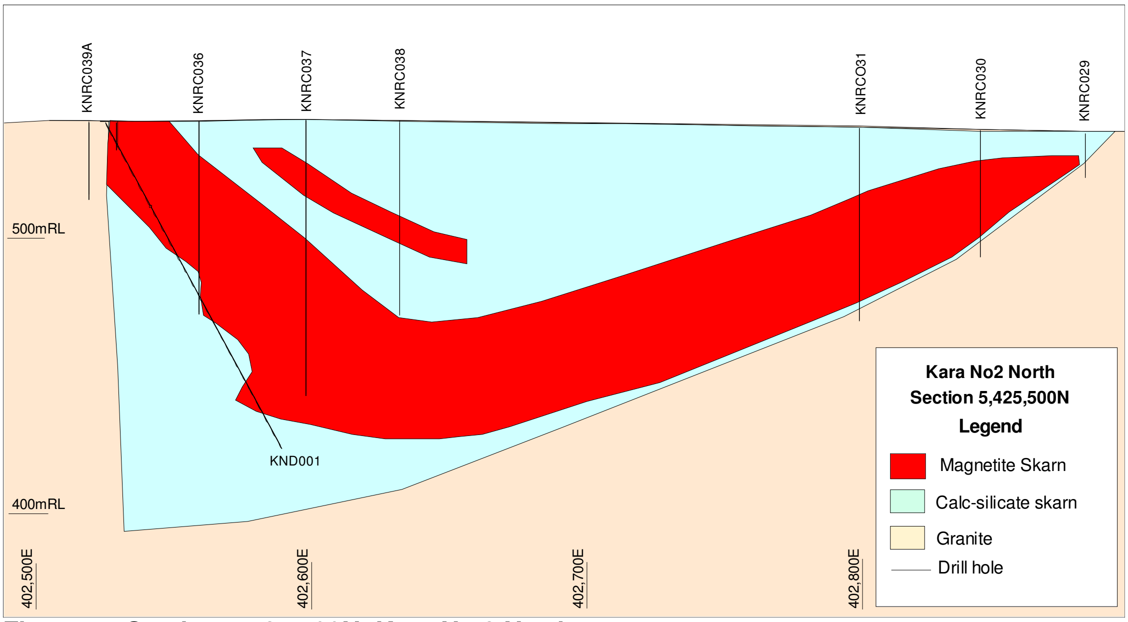

Figure 4. Section 5,425,500N, Kara No 2 North.

Other magnetite mineralisation within the Kara No 2 locality includes the Kara No 2 East, Kara No 2 South and Button Grass deposits. All of these skarns have been explored to varying degrees with outcropping magnetite skarn mineralisation of potentially economic widths and grades identified in all three. These deposits require further exploration drilling and are likely to provide additional resources to the project.

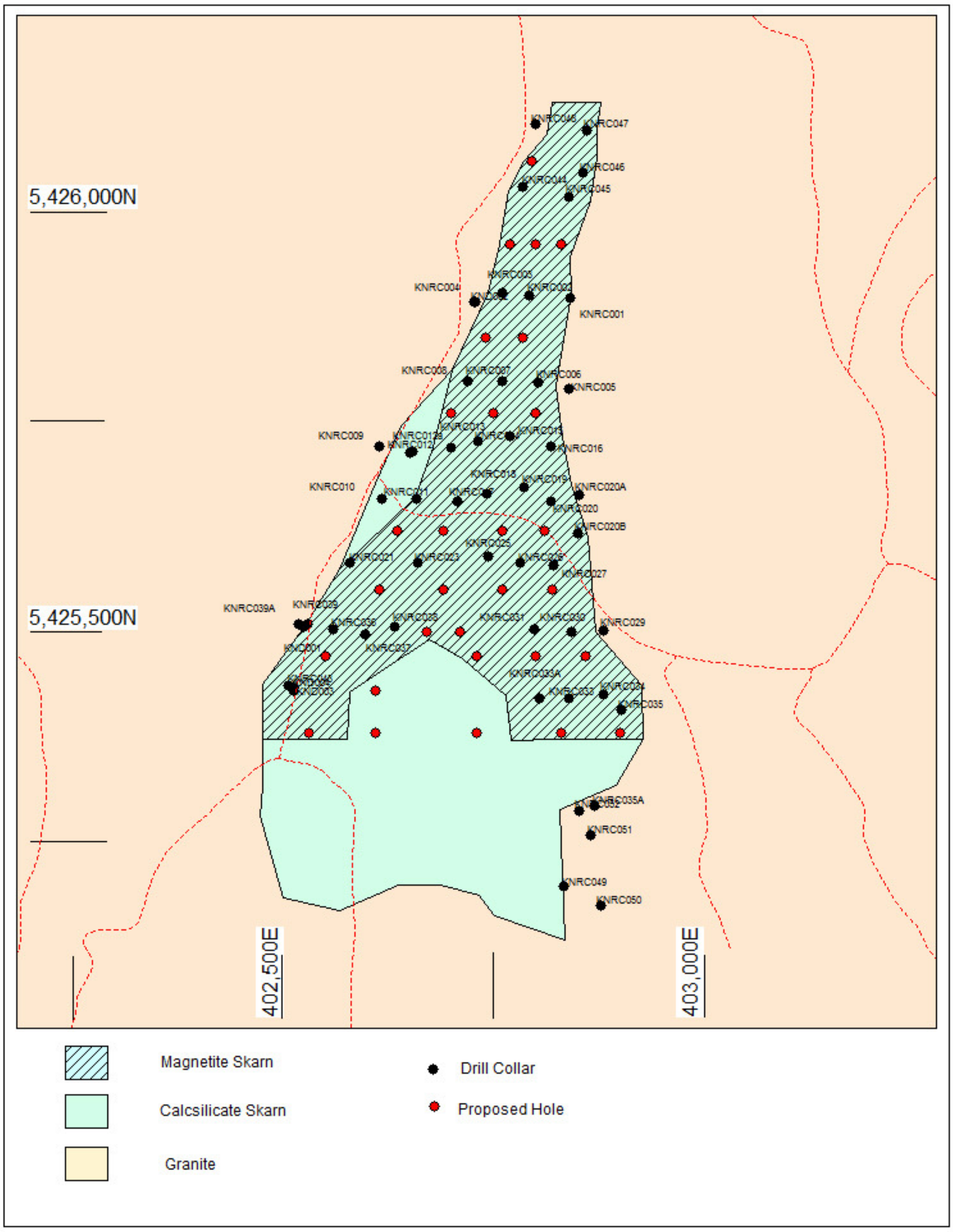

Figure 5. Kara 2 North Geology Plan and drill hole location.

3 DRILLING DATA

Drilling of the Kara No 2 North deposit consists of 51 RC holes for 2204m and 4 diamond drill holes for 444.9m. All of the RC holes and the first two diamond holes were drilled in an extensive exploration program in 2008 with an additional 2 diamond holes drilled in 2009. All of the drilling was completed by contract drilling company E-Drill.

Drill logs were entered on Tuffbook laptops in the field using excel spreadsheets. Lithological codes used by RVR have been migrated to the same as those used by Tasmania Mines to maintain consistency within the district. All RC holes have magnetic susceptibility logged downhole.

No downhole surveys were completed, presumably due to the lack of availability of gyroscopic survey instruments in Tasmania. Because of the short hole lengths, block size used for the estimation and style of mineralisation it is unlikely that the lack of downhole surveys will have a material impact on the estimation.

Drill hole sampling was incomplete down many RC holes with some intervals with lower magnetic susceptibility or poor sample recoveries of 3-5m not assayed within mineralised domains. The lack of data for these small internal low grades zones may result in a local overestimation of grade, however their small size is more than offset by magnetite mineralisation not included in the interpolation. It is considered that these zones are unlikely to have a material impact on global resource estimation.

All analyses were completed by AMMTECH laboratories in Burnie. All Fe is recorded as total iron and not magnetic iron. No Davis Tube Recoveries (DTR) were completed to determine recoverable magnetite. The requirement to estimate the magnetic and non-magnetic (hematite and iron-silicate) proportions is necessary to calculate recoverable tonnes and for model-mill reconciliations.

An updated and validated version of the drill database is located in digital format in the disc provided with the appendices.

Independent Laboratory checks were instigated as part of this resource estimation with bulk coarse rejects sent to SGS Laboratories in Perth. No appreciable bias was present in ore grade samples. There was a minor negative bias in low (<2%) Fe but this will not impact resource estimation. Data is located in Appendix 6.

Table 3. Summary of Kara No 2 North Drilling, Sampling Techniques and Data	
Criteria	**Status**
Drilling Techniques	• 4 diamond HQ and NQ diamond core for 444.9m • 51 RC drill holes for 2204m
Sample recovery	• Logged as poor, medium or high. 17% of samples recorded as poor, generally when water was encountered or near the top of the hole in weathered skarn.
Logging	• Geological logs on excel spreadsheets.
Sub-Sample preparation	• Half core split by diamond saw on 1m samples while respecting geological contacts for DDH. • 2kg sub-sample speared from bulk RC samples.
Sample preparation	• Crushed and pulverized to 70 micron at Burnie AMTECH laboratories.
Sample Analysis	• *XRF fusion disc for multi element analysis* • ***No Davis Tube Recoveries completed***
Assay QA/QC	• ***No QA/QC program was implemented with the RVR drilling programs.*** • ***No Independent laboratory analyses have been completed during drilling campaigns. Independent laboratory check analyses have been instigated as part of this resource estimation.*** • ***It is recommended that QA/QC programs be instigated for future drilling programs. Independent laboratory tests will be completed on sample pulps available.***
Location of Data	• All hole collar surveys by GPS. • All coordinates in GDA94 Zone 55. • No Down hole surveys recorded
Data Spacing and distribution	• Drill spacing approximately 100 x 50. • The majority of DDH have been drilled west-east or vertical, sub-perpendicular to ore body strike.
Database Integrity	• All data captured and stored in customised access database and validated and updated by REG 2011. • All historic drill logs entered into excel spreadsheets prior to being downloaded into database. Lithology codes migrated to Tasmania Mines codes. • Data integrity validated with Surpac Software for EOH depth and sample overlaps. • Manual check by reviewing cross sections with the historic drafted sections and plans.

4 MINERAL RESOURCE ESTIMATION

The Kara No 2 North Mineral Resource has been derived from a kriged block model created with Surpac^{tm} software licensed to Tim Callaghan. The block model extends between 5,425,100 to 5,426,200N, 402,300 to 403,100E and 300 to 600m RL.

4.1 GEOLOGICAL DOMAINING

Wire-framed solid models of geological and mineralisation domains were created from 50-100m spaced east-west cross sections utilizing drill hole data, aeromagnetic images, ground-magnetic maps and historic (1982) 1:10,000 geological maps. A digital terrain Model DTM was created from 10 topographic contours and drill collar surveys.

Mineralized Fe domains are delineated using a minimum mining width of 5m @ 25% Fe with some allowances for geological continuity. Internal dilution was restricted to a maximum of 5m where possible, again maintaining geological continuity. Drillhole assaying of some RC holes is not complete, either due to poor recoveries or due to deliberate omissions by field geologists. Magnetic susceptibility readings were completed on each metre sample as well as a visual estimation of magnetite content. Where assay data was incomplete, domain boundaries have been selected by magnetic susceptibility readings of >100si units, corresponding with logged magnetite skarn.

Solid models have been 'snapped' to drill holes where possible to accurately capture and model data and eliminate sectional projection inaccuracies.

Solid models created include:

- Digital Terrain Model dtm_gda94.dtm
- Granite Boundary grad.dtm
- Magnetite Skarn skmg.dtm
- Base of oxidation base_ox.dtm

The digital terrain model (DTM) was created from Lands Department 10m topographic contours and surveyed collar locations. The DTM has a vertical error of 5m and is not suitable for detailed engineering. A site survey is recommended to create a suitable DTM for future pit optimization and reserve definition.

4.2 COMPOSITING OF DATA

Data used for this estimation has been derived from reverse circulation (80%) and diamond drill holes (20%).

Drill hole intercepts of solid models have been flagged with Surpac Software and relevant intervals stored in the access database. Drill hole data has been composited on 1m lengths. Composites of less than 0.25m were not included in statistical studies or in the resource estimate.

Composited data is located in Appendix 1 and as .csv files on the attached data disc.

4.3 SAMPLE STATISTICAL STUDIES

The mean Fe grade for the diamond holes was 37.8% and for the RC holes was 37% with standard deviation of 12 and 11 respectively, suggesting there is no appreciable bias between drilling techniques.

Descriptive statistics and histograms of composited data are located in Table 4, and in Figure 6 and in Appendix 2.

Table 4. Kara No2 North 1m Composite Statistics

Variable	Fe %	SnO2 %	WO3 %	CaO %	P2O5%	SO3 %
Number of samples	861	838	685	687	684	521
Minimum value	1.15	0.01	0.01	0.15	0.002	0.01
Maximum value	67.01	0.76	0.41	43.00	0.25	19.60
Mean	37.01	0.09	0.08	14.81	0.04	0.36
Median	35.90	0.08	0.07	15.00	0.03	0.03
Geometric Mean	34.99	0.07	0.07	12.21	0.03	0.06
Variance	131.53	0.007	0.002	49.74	0.001	2.22
Standard Deviation	11.47	0.08	0.05	7.05	0.03	1.49
Coefficient of variation	0.31	0.89	0.57	0.48	0.83	4.12
Skewness	0.16	3.14	1.59	-0.01	2.21	8.47
Kurtosis	2.44	18.80	8.34	2.58	9.98	87.83
Natural Log Mean	3.56	-2.67	-2.65	2.50	-3.53	-2.88
Log Variance	0.13	0.65	0.35	0.60	0.63	2.39

Magnetite skarn mineralisation 1m composite Fe grades have an essentially normal distribution with a slight positive skew and a low coefficient of variation. WO_3 and P_2O_5 composites within the magnetite skarn domains demonstrate a moderately skewed distribution with a small high grade tail (Appendix 2). CaO composites demonstrate an essentially normal distribution. SnO_2 and SO_3 composites within the magnetite skarn domains have a strongly positively skewed distribution with high grade outliers. With the exception of SO_3, all variables have a low coefficient of variation and no top cutting was considered necessary. A top cut of 1.0% SO_3 was applied to the 1m Composites based on the 95th percentile. Further domain modeling of discreet high sulphide zones is recommended for future estimations.

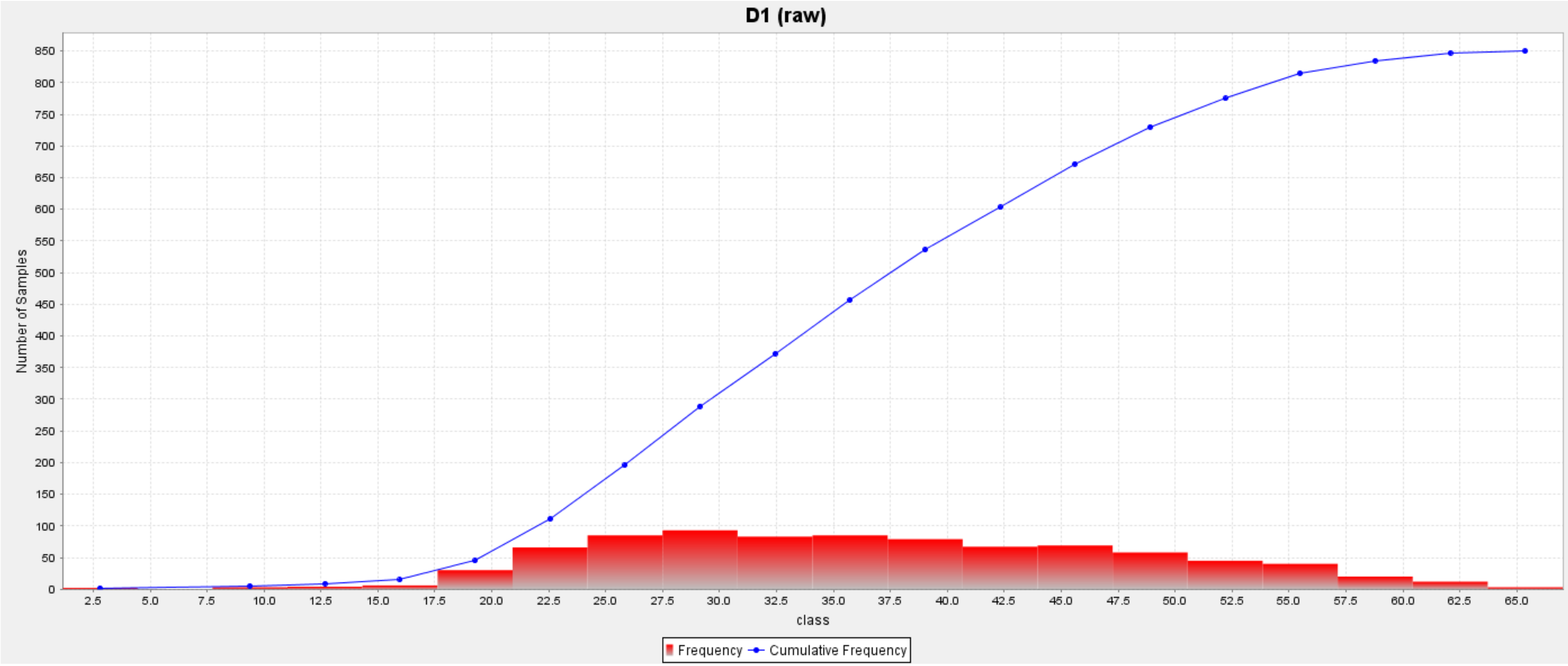

Figure 6. Cumulative frequency histogram of Kara No 2 North 1m composite Fe % grades.

4.4 VARIOGRAM MODELING

Variography of 1m composited data was modeled using Surpac Software and variogram models are located in Appendix 3 and Figure 7. Variogram models were constructed from 1m composited data. There is insufficient data to warrant directional variography. Horizontal semi-variograms were constructed with a N-S search and a spread of 30°.

Downhole semi-variograms typically displayed low to moderate nugget effect and short ranges of 3.8 to 16m to the first structure (except WO_3, 28.6m) and typically long ranges of between 30-60m to the second structure of nested spherical models (Table 5 and Appendix 3).

Table 5. Downhole Semi-variogram Parameters (spherical and nested spherical models).

Variable	Nugget	Sill	Range	Major:semi	Major:minor
Fe %	18.1	53 57	4.5 68	1 1	1 1
SnO_2 %	0.0006	0.0022 .0038	3.8 39.8	1 1	1 1
WO_3 %	0.0006	0.016	28.6	1	1
CaO %	6.3	19.9 22.9	6.5 52.3	1 1	1 1
P_2O_5 %	0.0002	0.0008	7.5	1	1
SO_3 %	0	2.6	16	1	1

Horizontal semi-variograms typically displayed long ranges of over 100m (Table 6 and Appendix 3).

Table 6. Horizontal Semi-variogram Parameters (spherical models).

Variable	Nugget	Sill	Range	Major:semi	Major:minor
Fe %	18.1	111	122	1	1
SnO_2 %	0.0006	0.005	151	1	1
WO_3 %	0.0006	0.002	105	1	1
CaO %	6.3	43	126	1	1
P_2O_5 %	0.0002	0.001	105	1	1
SO_3 %	0	2.6	157	1	1

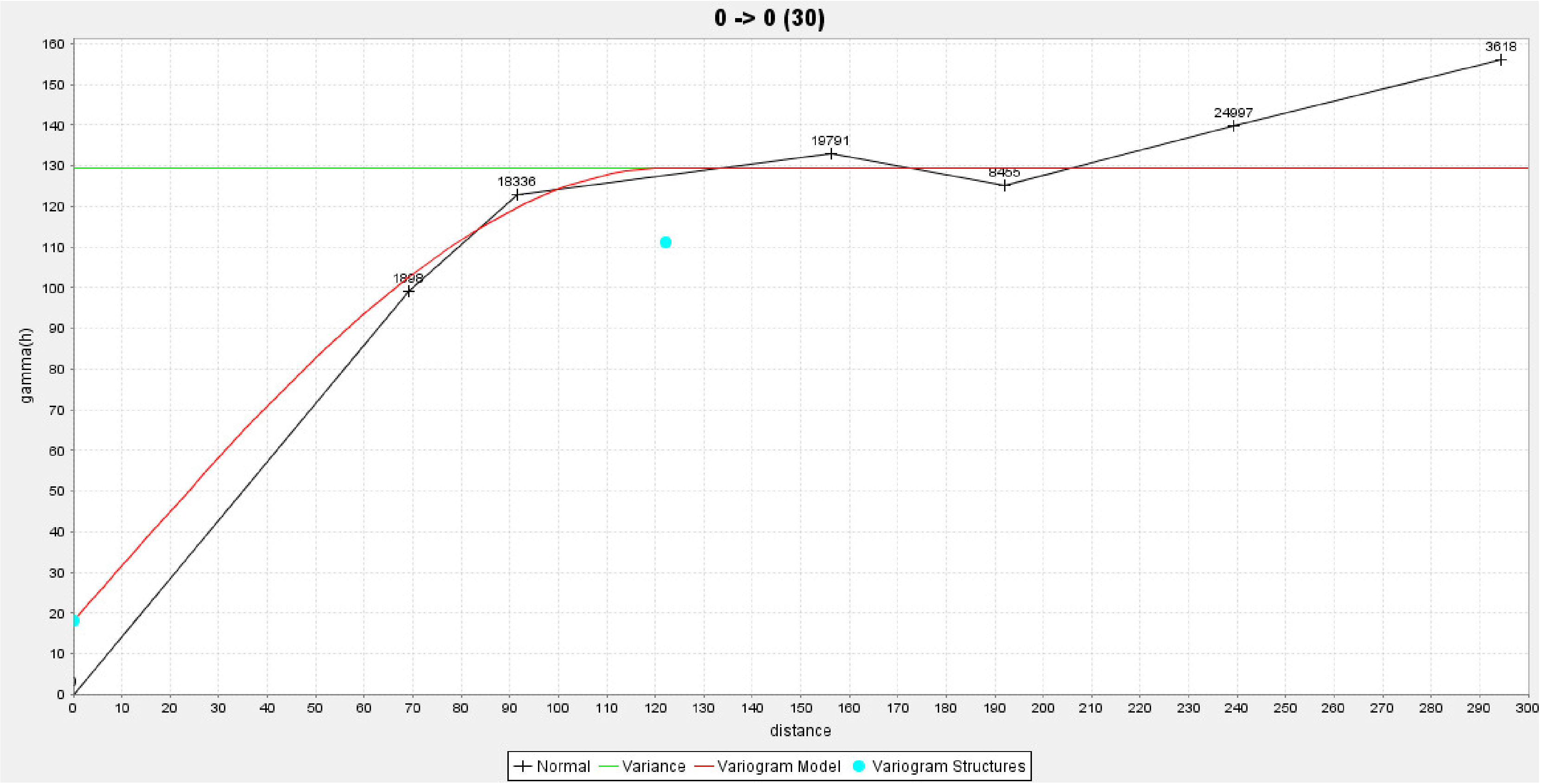

Figure 7. Horizontal variogram model for Kara No 2 North Fe.

4.5 RESOURCE ESTIMATION PROCEDURE.

The Kara 2 North grades have been interpolated into a blockmodel using an ordinary kriging algorithm. Block sizes were set at 20m x 20m x 5m with sub-celling to 2.5m in the x, y and 1.25 in the z direction to ensure model volume resolution. Parent block sizes were selected to be approximately half the east-west drill spacing.

Zone codes assigned to blocks contained within the separate geological domains include:

- Granite = 1
- Calc-silicate skarn = 2
- Magnetite skarn = 3

Spherical variogram model parameters used for each domain are outlined in Table 6. An elliptical search was undertaken. Search neighborhood parameters used for interpolation are listed in Table 7.

Table 7. Search Neighborhood Parameters	
Ellipse plunge	0°
Ellipse bearing	0°
Ellipse dip	0°
Search Radius	200m
Major:semi major ratio	1
Major:minor ratio	1
Discretisation points	3:3:3
Minimum No of samples	4
Maximum No of samples	10

4.6 BULK DENSITY

No bulk density measurements were completed during the drilling campaigns nor were any reports specifically detailing SG estimation cited. A limited program of bulk density determination was completed as part of this resource estimation. A total of 90 measurements were made on quartered diamond drill core from diamond drill holes KND002, KND003 and KND004 using the Archimedes method. The samples returned an average bulk density of 4.0 with a minimum of 2.9 and a maximum of 4.9 with a standard deviation of 0.4. Bulk density data is located in Appendix 6.

Bulk Densities for the three main mineralogical domains includes:

Granite	SG = 2.6
Calc silicate skarn	SG = 3.2
Magnetite skarn	SG = 4.0

As a check on bulk density determinations, a theoretical bulk density of 4.0 was determined from literature on specific mineral compositions (Deer, Howie and Zussman, 1966). The Magnetite Skarn bulk density was calculated using a ratio of 40% magnetite to 60% diopside:

$$\text{Bulk Density} = (0.4 \times SGmag) + (0.6 \times SGdiop) = 4.0$$

Where $SGmag = 5.2$ and $SGdiop = 3.2$

Tasmania Mines Kara No1 deposit has a bulk density of 4.1 which suggests the methodology used for this estimation is reasonable.

Due to the variable nature of skarn formation it is likely there will be considerable variance in the bulk density of the ore.

It is recommended that systematic bulk density determinations be made on future diamond drilling programs.

6 RESULTS

The total estimated Mineral Resource for the magnetite skarn within the Kara No 2 North deposit, classified as Inferred Resource in accordance with the 2004 JORC Code is located in Table 8.

Table 8. Kara No 2 North Inferred Resource

	MTonnes	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
Oxidised	2.15	42.1	0.10	0.10	11.0	0.04	0.08
Un-oxidised	14.47	36.7	0.08	0.08	16.1	0.03	0.28
Total	**16.62**	**37.4**	**0.08**	**0.08**	**15.4**	**0.03**	**0.25**

The mineral resource includes 16.62 Mt of un-oxidised magnetite skarn mineralisation and 2.15 Mt of weathered magnetite skarn.

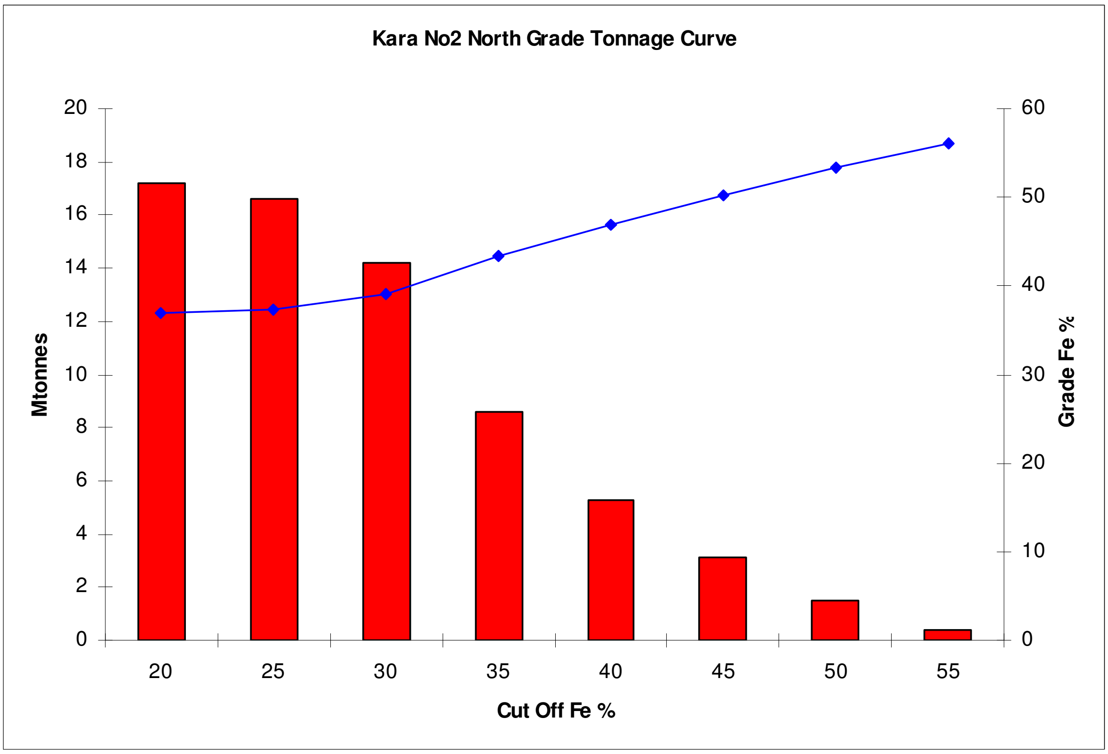

Figure 8. Kara No 2 North Grade Tonnage Curve

6.1 CLASSIFICATION

The similarities between this style of mineralisation and Tasmania Mines operations provide confidence in the resource estimation, despite the lack of DTR analyses, bulk density data and QA/QC programs.

The resource has been classified as an Inferred Resource in accordance with the 2004 edition of the JORC code because:

- Drill spacing of 100m section is considered insufficient to adequately define the variability of this style of mineralisation.
- There is no QA/QC data available from the drilling programs
- There are only limited Bulk Density determinations from the drilling programs
- No Davis Tube Recoveries were completed to quantify the recoverable magnetite content

6.2 VALIDATION

The wireframe volume of 4.32Mm^3 reconciles well with the blockmodel mineralisation volume of 4.29Mm^3.

The Blockmodelled grades were validated with the drillhole assays visually on cross sections with no obvious bias apparent. Internal low grade zones correspond with estimated low grade blocks.

The estimated grade for the Fe mineralisation of 37.4% reconciles well with the composite average of 37.1% Fe. Similarly the estimated grades for SnO_2, WO_3, CaO and P_2O_5 reconcile well with the 1m composite mean and median grades. The estimation for SO_3 within the model would benefit from separate domaining of the minor discreet zones of sulphide mineralisation within the skarn.

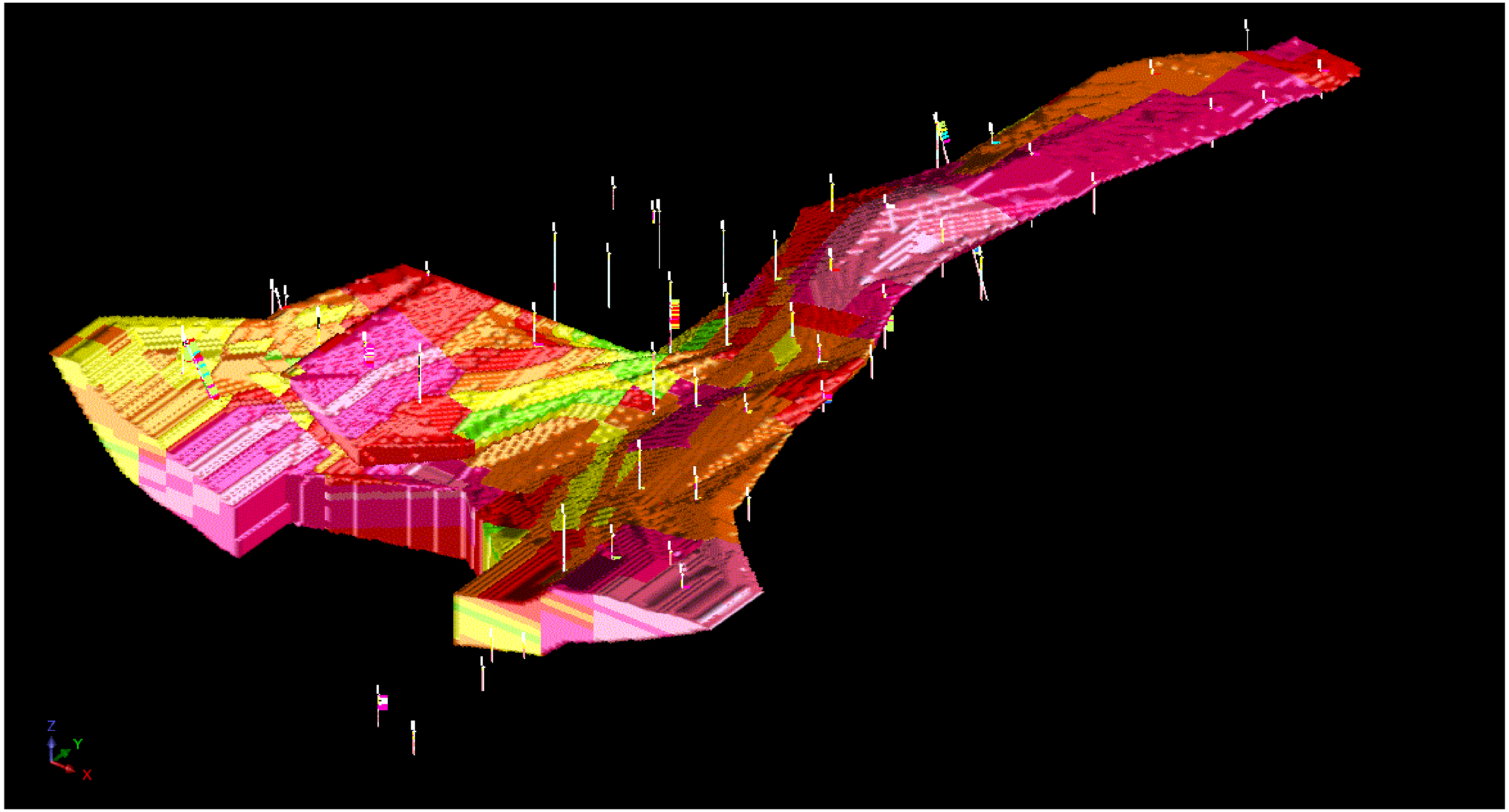

Figure 9. Kara No 2 North Blockmodel, looking NW. Inferred Resource of 16.62Mt @ 37.4% Fe.

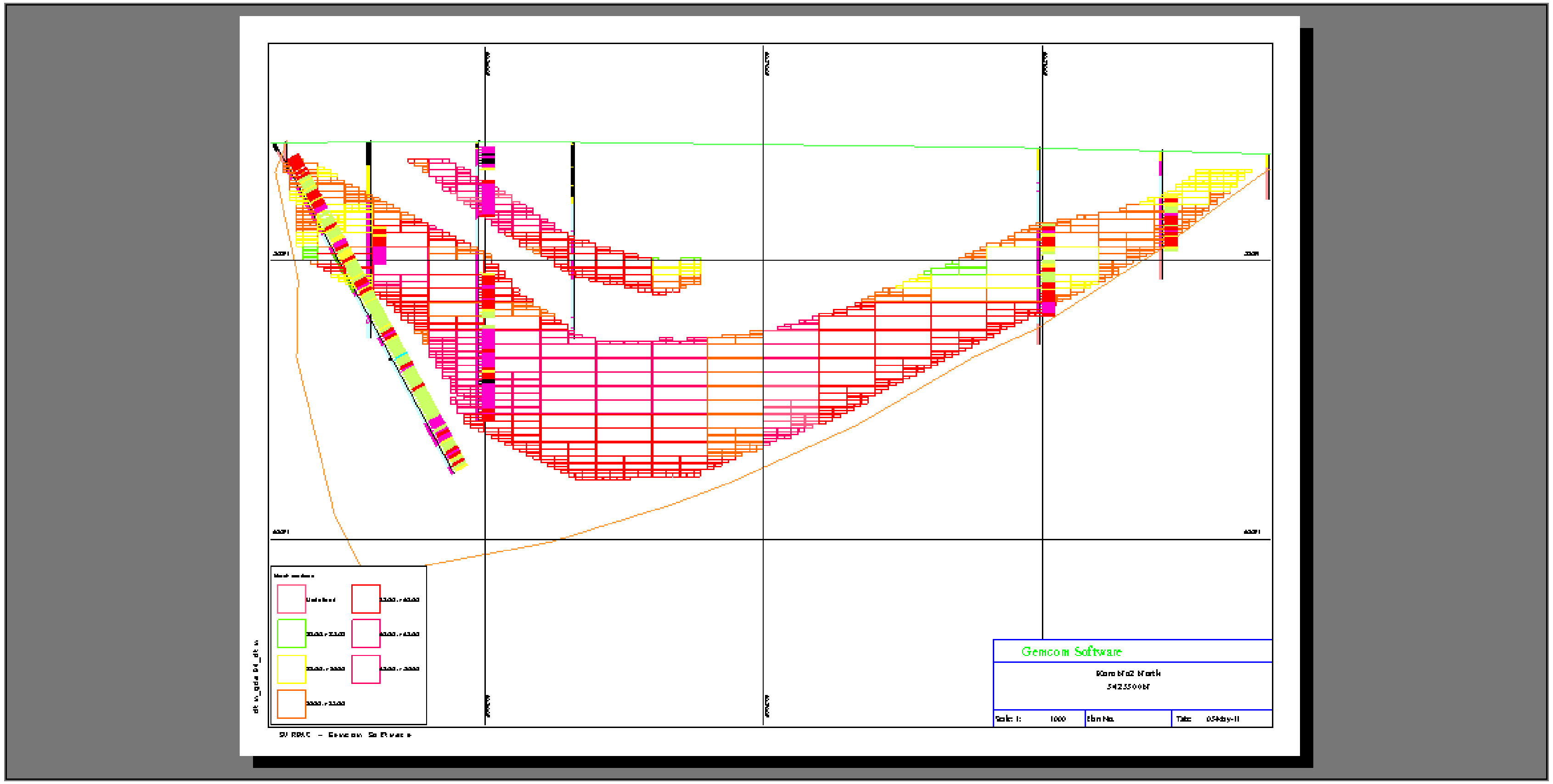

Figure 10. Section 5,425,500N, Kara No 2 North block model.

8 RECOMMENDATIONS

The Kara No 2 North deposit requires infill drilling on nominally 50m spacing to adequately test the deposit before Measured and Indicated Resource estimation and Reserve Definition can be completed. It is recommended that future drilling programs use HQ diamond core if possible to improve sample recoveries and provide samples suitable for metallurgical testwork and geotechnical investigations.

Sampling of RC drilling within magnetite skarn mineralisation is incomplete. Mineralisation domains were based primarily on the Fe grade but have also been constructed on the lithological log and the magnetic susceptibility readings to allow for inconsistent sampling. It is recommended that sampling of future drilling programs be completed continuously through mineralisation zones and extending 1-3m either side of magnetite skarn zones in accordance with industry standard best practice.

An additional 4000m of drilling (preferably diamond drilling) is estimated to bring the Kara No 2 Skarn to Measured and Indicated status. The drilling program is estimated to cost approximately $0.9M.

Recommendations for future work include:

- Infill drilling to 50m spaced sections.
- Geotechnical logging of future drilling campaigns
- Bulk Density measurements on diamond drill core.
- Davis Tube Recoveries and metallurgical testwork on drill core samples
- Initiation of a QA/QC regime in future drilling programs.
- Estimation of Measured and Indicated Mineral Resource
- Pit optimization studies and reserve definition.
- Resource extension and exploration drilling.
- Sterilisation drilling of proposed infrastructure locations.

Further technical studies required include resource estimation, reserve definition, geotechnical investigations and metallurgical testwork. These technical programs should be completed concurrently with the drilling program to form the basis of a feasibility study.

ADDITIONAL NOTES

LIMITATIONS AND CONSENT

The report is provided to Forward Mining Ltd in the context of a Mineral Resource Estimation and should not be used or relied upon for any other purpose.

This report has been prepared using information available to the Author at the time of writing. The opinions stated herein are given in good faith and with the belief that the basic assumptions are factual and correct and the interpretations reasonable.

This report is not intended for use as a public document nor, in whole or in part, in a public document without written consent to the form and context in which it appears.

COMPETENT PERSON AND JORC CODE

This report was prepared in accordance with the 2004 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves' ("JORC Code") by Tim Callaghan, who is a Member of The Australian Institute of Mining and Metallurgy ("AusIMM"), has a minimum of five years experience in the estimation and assessment and evaluation of Mineral Resources of this style and is the competent Person as defined in the JORC Code. This announcement accurately summarises and fairly reports his estimations and he has consented to the resource report in the form and context it appears.

STATEMENT OF INDEPENDENCE

Tim Callaghan has no material interest or entitlement in the securities or assets of the Forward Mining Ltd or any associated companies.

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Appendix 1

Kara No 2 North 1m Composites

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KND001	7	8	5,425,504.7	402,528.5	535.4	33.5	0.18				
KND001	8	9	5,425,504.5	402,529.0	534.6	34.2	0.16				
KND001	9	10	5,425,504.4	402,529.5	533.7	34.1	0.19				
KND001	10	11	5,425,504.2	402,529.9	532.8	36.6	0.11				
KND001	11	12	5,425,504.0	402,530.4	532.0	33.8	0.12				
KND001	12	13	5,425,503.9	402,530.9	531.1	37.6	0.25				
KND001	13	14	5,425,503.7	402,531.3	530.2	37.6	0.25				
KND001	14	15	5,425,503.5	402,531.8	529.4	33.46	0.262				
KND001	15	16	5,425,503.3	402,532.3	528.5	25.72	0.246				
KND001	16	17	5,425,503.2	402,532.8	527.6	24.98	0.182				
KND001	17	18	5,425,503.0	402,533.2	526.8	23.4	0.216				
KND001	18	19	5,425,502.8	402,533.7	525.9	23.12	0.212				
KND001	19	20	5,425,502.7	402,534.2	525.0	25.12	0.354				
KND001	20	21	5,425,502.5	402,534.6	524.2	24.28	0.356				
KND001	21	22	5,425,502.3	402,535.1	523.3	32.58	0.688				
KND001	22	23	5,425,502.2	402,535.6	522.4	34.68	0.708				
KND001	23	24	5,425,502.0	402,536.0	521.6	32.54	0.582				
KND001	24	25	5,425,501.8	402,536.5	520.7	30.2	0.466				
KND001	25	26	5,425,501.6	402,537.0	519.8	33.02	0.28				
KND001	26	27	5,425,501.5	402,537.5	519.0	36.88	0.226				
KND001	27	28	5,425,501.3	402,537.9	518.1	42.56	0.206				
KND001	28	29	5,425,501.1	402,538.4	517.2	44.68	0.208				
KND001	29	30	5,425,501.0	402,538.9	516.4	32.34	0.19				
KND001	30	31	5,425,500.8	402,539.3	515.5	24.7	0.17				
KND001	31	32	5,425,500.6	402,539.8	514.6	24.7	0.17				
KND001	32	33	5,425,500.4	402,540.3	513.8	23.62	0.14				
KND001	33	34	5,425,500.3	402,540.7	512.9	23.8	0.114				
KND001	34	35	5,425,500.1	402,541.2	512.0	21.22	0.128				
KND001	35	36	5,425,499.9	402,541.7	511.2	27.38	0.128				
KND001	36	37	5,425,499.8	402,542.1	510.3	30.98	0.112				
KND001	37	38	5,425,499.6	402,542.6	509.4	24.65	0.12				
KND001	38	39	5,425,499.4	402,543.1	508.6	21.83	0.126				
KND001	39	40	5,425,499.2	402,543.6	507.7	17.1	0.16				
KND001	40	41	5,425,499.1	402,544.0	506.8	28.4	0.16				
KND001	41	42	5,425,498.9	402,544.5	506.0	25.5	0.17				
KND001	42	43	5,425,498.7	402,545.0	505.1	45.5	0.19				
KND001	43	44	5,425,498.6	402,545.4	504.2	49.1	0.17				
KND001	44	45	5,425,498.4	402,545.9	503.4	31.2	0.2				
KND001	45	46	5,425,498.2	402,546.4	502.5	19.6	0.14				
KND001	46	47	5,425,498.0	402,546.8	501.7	25.9	0.17				
KND001	47	48	5,425,497.9	402,547.3	500.8	25.3	0.17				
KND001	48	49	5,425,497.7	402,547.8	499.9	29.1	0.12				
KND001	49	50	5,425,497.5	402,548.3	499.1	33.2	0.11				
KND001	50	51	5,425,497.4	402,548.7	498.2	27.4	0.14				
KND001	51	52	5,425,497.2	402,549.2	497.3	23.6	0.11				
KND001	52	53	5,425,497.0	402,549.7	496.5	16.3	0.14				
KND001	53	54	5,425,496.9	402,550.1	495.6	20	0.17				
KND001	54	55	5,425,496.7	402,550.6	494.7	19.6	0.16				
KND001	55	56	5,425,496.5	402,551.1	493.9	19.4	0.17				

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KND001	56	57	5,425,496.3	402,551.5	493.0	27.2	0.11				
KND001	57	58	5,425,496.2	402,552.0	492.1	11.9	0.07				
KND001	58	59	5,425,496.0	402,552.5	491.3	30.9	0.14				
KND001	59	60	5,425,495.8	402,553.0	490.4	32.6	0.16				
KND001	60	61	5,425,495.7	402,553.4	489.5	41.1	0.15				
KND001	61	62	5,425,495.5	402,553.9	488.7	28.2	0.14				
KND001	62	63	5,425,495.3	402,554.4	487.8	31.3	0.11				
KND002	43.3	44.3	5,425,884.5	402,747.6	508.9	42.42	0.083				
KND002	44.3	45.3	5,425,884.3	402,748.0	508.1	56.04	0.09				
KND002	45.3	46.3	5,425,884.2	402,748.5	507.2	56.13	0.093				
KND002	46.3	47.3	5,425,884.0	402,749.0	506.4	45.98	0.094				
KND002	47.3	48.3	5,425,883.8	402,749.5	505.5	41.48	0.086				
KND002	48.3	49.3	5,425,883.7	402,749.9	504.6	47.1	0.106				
KND002	49.3	50.3	5,425,883.5	402,750.4	503.8	51.65	0.108				
KND002	50.3	51.3	5,425,883.3	402,750.9	502.9	50.79	0.086				
KND002	51.3	52.3	5,425,883.1	402,751.3	502.0	53.99	0.1				
KND002	52.3	53.3	5,425,883.0	402,751.8	501.2	48.84	0.106				
KND002	53.3	54.3	5,425,882.8	402,752.3	500.3	37.35	0.117				
KND002	54.3	55.3	5,425,882.6	402,752.7	499.4	34.29	0.11				
KND002	55.3	56.3	5,425,882.5	402,753.2	498.6	35.74	0.125				
KND002	56.3	57.3	5,425,882.3	402,753.7	497.7	29.81	0.148				
KND002	57.3	58.3	5,425,882.1	402,754.2	496.8	32.24	0.132				
KND002	58.3	59.3	5,425,881.9	402,754.6	496.0	26.67	0.154				
KND002	59.3	60.3	5,425,881.8	402,755.1	495.1	35.16	0.131				
KND002	60.3	61.3	5,425,881.6	402,755.6	494.2	44.59	0.107				
KND002	61.3	62.3	5,425,881.4	402,756.0	493.4	57.5	0.106				
KND002	62.3	63.3	5,425,881.3	402,756.5	492.5	58.41	0.114				
KND002	63.3	64.3	5,425,881.1	402,757.0	491.6	62.27	0.1				
KND002	64.3	65.3	5,425,880.9	402,757.4	490.8	55.43	0.115				
KND002	65.3	66.3	5,425,880.7	402,757.9	489.9	42.6	0.1495				
KND002	66.3	67.3	5,425,880.6	402,758.4	489.0	53.9	0.141				
KND002	67.3	68.3	5,425,880.4	402,758.9	488.2	54.54	0.1				
KND002	68.3	69.3	5,425,880.2	402,759.3	487.3	48.88	0.116				
KND002	69.3	70.3	5,425,880.1	402,759.8	486.4	48.61	0.116				
KND002	70.3	71.3	5,425,879.9	402,760.3	485.6	41	0.142				
KND002	71.3	72.3	5,425,879.7	402,760.7	484.7	22.04	0.087				
KND002	72.3	73.3	5,425,879.6	402,761.2	483.8	26.66	0.2385				
KND003	25.9	26.9	5,425,440.1	402,503.5	520.5	29.7	0.06				
KND003	26.9	27.9	5,425,440.5	402,503.2	519.7	23	0.05				
KND003	27.9	28.9	5,425,440.9	402,502.9	518.8	24.02	0.046				
KND003	28.9	29.9	5,425,441.3	402,502.6	517.9	27.84	0.106				
KND003	29.9	30.9	5,425,441.6	402,502.2	517.1	39.02	0.168				
KND003	30.9	31.9	5,425,442.0	402,501.9	516.2	43.66	0.296				
KND003	31.9	32.9	5,425,442.4	402,501.6	515.3	44.44	0.482				
KND003	32.9	33.9	5,425,442.8	402,501.3	514.5	45.64	0.392				
KND003	33.9	34.9	5,425,443.2	402,500.9	513.6	21.55	0.125				
KND003	34.9	35.9	5,425,443.6	402,500.6	512.7	1.4	0.015				
KND003	35.9	36.9	5,425,443.9	402,500.3	511.9	1.15	0.015				
KND003	36.9	37.9	5,425,444.3	402,500.0	511.0	13.07	0.047				

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KND003	37.9	38.9	5,425,444.7	402,499.7	510.1	40.19	0.23				
KND003	38.9	39.9	5,425,445.1	402,499.3	509.3	40.49	0.438				
KND003	39.9	40.9	5,425,445.5	402,499.0	508.4	45.69	0.315				
KND003	40.9	41.9	5,425,445.9	402,498.7	507.5	40.08	0.429				
KND003	41.9	42.9	5,425,446.2	402,498.4	506.7	26.98	0.408				
KND004	29.5	30.5	5,425,432.0	402,727.0	517.3	32.23	0.115				
KND004	30.5	31.5	5,425,432.0	402,727.5	516.5	44.95	0.165				
KND004	31.5	32.5	5,425,432.0	402,728.0	515.6	34.6	0.165				
KND004	32.5	33.5	5,425,432.0	402,728.5	514.7	25.6	0.135				
KND004	33.5	34.5	5,425,432.0	402,729.0	513.9	25.05	0.115				
KND004	34.5	35.5	5,425,432.0	402,729.5	513.0	22.35	0.13				
KND004	35.5	36.5	5,425,432.0	402,730.0	512.1	22.85	0.165				
KND004	36.5	37.5	5,425,432.0	402,730.5	511.3	33.65	0.165				
KND004	37.5	38.5	5,425,432.0	402,731.0	510.4	39.8	0.145				
KND004	38.5	39.5	5,425,432.0	402,731.5	509.5	33.75	0.14				
KND004	39.5	40.5	5,425,432.0	402,732.0	508.7	28.3	0.14				
KND004	40.5	41.5	5,425,432.0	402,732.5	507.8	23.76	0.128				
KND004	41.5	42.5	5,425,432.0	402,733.0	506.9	26.67	0.1				
KND004	42.5	43.5	5,425,432.0	402,733.5	506.1	30.9	0.1				
KND004	43.5	44.5	5,425,432.0	402,734.0	505.2	29.5	0.1				
KND004	44.5	45.5	5,425,432.0	402,734.5	504.3	31.5	0.1				
KND004	45.5	46.5	5,425,432.0	402,735.0	503.5	29.2	0.1				
KND004	46.5	47.5	5,425,432.0	402,735.5	502.6	34.6	0.11				
KND004	47.5	48.5	5,425,432.0	402,736.0	501.7	38.2	0.09				
KND004	48.5	49.5	5,425,432.0	402,736.5	500.9	45.1	0.09				
KND004	49.5	50.5	5,425,432.0	402,737.0	500.0	39.4	0.14				
KND004	50.5	51.5	5,425,432.0	402,737.5	499.1	33.3	0.16				
KND004	51.5	52.5	5,425,432.0	402,738.0	498.3	30	0.12				
KND004	52.5	53.5	5,425,432.0	402,738.5	497.4	46.3	0.09				
KND004	53.5	54.5	5,425,432.0	402,739.0	496.5	48.3	0.1				
KND004	54.5	55.5	5,425,432.0	402,739.5	495.7	44.9	0.12				
KND004	55.5	56.5	5,425,432.0	402,740.0	494.8	49.15	0.105				
KND004	56.5	57.5	5,425,432.0	402,740.5	493.9	56.95	0.08				
KND004	57.5	58.5	5,425,432.0	402,741.0	493.1	60.55	0.075				
KND004	58.5	59.5	5,425,432.0	402,741.5	492.2	56.95	0.09				
KND004	59.5	60.5	5,425,432.0	402,742.0	491.3	54.25	0.1				
KND004	60.5	61.5	5,425,432.0	402,742.5	490.5	55.35	0.095				
KND004	61.5	62.5	5,425,432.0	402,743.0	489.6	49.7	0.1				
KND004	62.5	63.5	5,425,432.0	402,743.5	488.7	49.05	0.105				
KND004	63.5	64.5	5,425,432.0	402,744.0	487.9	49.7	0.11				
KND004	64.5	65.5	5,425,432.0	402,744.5	487.0	48.3	0.12				
KND004	65.5	66.5	5,425,432.0	402,745.0	486.1	51.2	0.12				
KND004	66.5	67.5	5,425,432.0	402,745.5	485.3	46.8	0.12				
KND004	67.5	68.5	5,425,432.0	402,746.0	484.4	43.8	0.115				
KND004	68.5	69.5	5,425,432.0	402,746.5	483.5	46.45	0.1				
KND004	69.5	70.5	5,425,432.0	402,747.0	482.7	48	0.09				
KND004	70.5	71.5	5,425,432.0	402,747.5	481.8	50.6	0.095				
KND004	71.5	72.5	5,425,432.0	402,748.0	480.9	55.25	0.09				
KND004	72.5	73.5	5,425,432.0	402,748.5	480.1	57.9	0.08				

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KND004	73.5	74.5	5,425,432.0	402,749.0	479.2	55.7	0.08				
KND004	74.5	75.5	5,425,432.0	402,749.5	478.3	48.6	0.095				
KND004	75.5	76.5	5,425,432.0	402,750.0	477.5	46.65	0.11				
KND004	76.5	77.5	5,425,432.0	402,750.5	476.6	49.35	0.115				
KND004	77.5	78.5	5,425,432.0	402,751.0	475.8	50.5	0.11				
KND004	78.5	79.5	5,425,432.0	402,751.5	474.9	52.3	0.1				
KND004	79.5	80.5	5,425,432.0	402,752.0	474.0	53.95	0.095				
KND004	80.5	81.5	5,425,432.0	402,752.5	473.2	57.9	0.085				
KND004	81.5	82.5	5,425,432.0	402,753.0	472.3	56.7	0.095				
KND004	82.5	83.5	5,425,432.0	402,753.5	471.4	55.35	0.1				
KND004	83.5	84.5	5,425,432.0	402,754.0	470.6	52.2	0.115				
KND004	84.5	85.5	5,425,432.0	402,754.5	469.7	48.8	0.125				
KND004	85.5	86.5	5,425,432.0	402,755.0	468.8	50.4	0.105				
KND004	86.5	87.5	5,425,432.0	402,755.5	468.0	47.25	0.095				
KND004	87.5	88.5	5,425,432.0	402,756.0	467.1	47.75	0.095				
KND004	88.5	89.5	5,425,432.0	402,756.5	466.2	50.55	0.105				
KND004	89.5	90.5	5,425,432.0	402,757.0	465.4	53.2	0.1				
KND004	90.5	91.5	5,425,432.0	402,757.5	464.5	50.4	0.095				
KND004	91.5	92.5	5,425,432.0	402,758.0	463.6	45.9	0.095				
KND004	92.5	93.5	5,425,432.0	402,758.5	462.8	47.55	0.1				
KND004	93.5	94.5	5,425,432.0	402,759.0	461.9	46.6	0.115				
KND004	94.5	95.5	5,425,432.0	402,759.5	461.0	45.4	0.12				
KND004	95.5	96.5	5,425,432.0	402,760.0	460.2	41.15	0.115				
KND004	96.5	97.5	5,425,432.0	402,760.5	459.3	32.25	0.105				
KNRC002	0	1	5,425,899.0	402,793.0	546.2	46.6	0.3	0.05	0.79	0.078	0.14
KNRC002	1	2	5,425,899.0	402,793.0	545.2	38	0.1	0.06	8.5	0.055	0.07
KNRC002	2	3	5,425,899.0	402,793.0	544.2	34.6	0.11	0.06	14.7	0.031	0.03
KNRC002	3	4	5,425,899.0	402,793.0	543.2	39	0.17	0.08	15.5	0.036	0.01
KNRC002	4	5	5,425,899.0	402,793.0	542.2	53.4	0.1	0.17	7.7	0.028	0.01
KNRC002	5	6	5,425,899.0	402,793.0	541.2	46	0.09	0.11	12.2	0.021	0.01
KNRC002	6	7	5,425,899.0	402,793.0	540.2	22.9	0.14	0.03	25.9	0.032	
KNRC002	7	8	5,425,899.0	402,793.0	539.2	55.6	0.03	0.15	6.3	0.022	0.01
KNRC002	8	9	5,425,899.0	402,793.0	538.2	46.4	0.06	0.11	9.5	0.03	0.03
KNRC002	9	10	5,425,899.0	402,793.0	537.2	28.6	0.22	0.04	24.8	0.042	
KNRC002	10	11	5,425,899.0	402,793.0	536.2	32.5	0.09	0.08	20.4	0.049	
KNRC002	11	12	5,425,899.0	402,793.0	535.2	31.2	0.14	0.06	20.9	0.042	
KNRC002	12	13	5,425,899.0	402,793.0	534.2	35.8	0.11	0.09	17.2	0.022	0.02
KNRC002	13	14	5,425,899.0	402,793.0	533.2	54.8	0.04	0.13	5.6	0.014	0.03
KNRC002	14	15	5,425,899.0	402,793.0	532.2	58.5	0.04	0.16	4.6	0.014	0.02
KNRC002	15	16	5,425,899.0	402,793.0	531.2	58.8	0.04	0.15	5.1	0.013	0.03
KNRC002	16	17	5,425,899.0	402,793.0	530.2	31	0.06	0.07	16.4	0.021	0.01
KNRC002	17	18	5,425,899.0	402,793.0	529.2	41.6	0.08	0.09	14.4	0.01	0.01
KNRC002	18	19	5,425,899.0	402,793.0	528.2	39.9	0.12	0.08	16.5	0.01	
KNRC002	19	20	5,425,899.0	402,793.0	527.2	36.1	0.12	0.07	16.7	0.012	0.02
KNRC002	20	21	5,425,899.0	402,793.0	526.2	45.5	0.13	0.1	13.6	0.009	0.01
KNRC002	21	22	5,425,899.0	402,793.0	525.2	40.5	0.11	0.07	15.7	0.01	
KNRC002	22	23	5,425,899.0	402,793.0	524.2	53.2	0.07	0.12	8	0.01	0.01
KNRC002	23	24	5,425,899.0	402,793.0	523.2	41.3	0.12	0.08	15.1	0.007	
KNRC002	24	25	5,425,899.0	402,793.0	522.2	42.7	0.09	0.07	13.3	0.027	

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC002	25	26	5,425,899.0	402,793.0	521.2	27.9	0.05	0.03	22.7	0.063	
KNRC002	26	27	5,425,899.0	402,793.0	520.2	31	0.03	0.04	19.7	0.045	0.02
KNRC002	27	28	5,425,899.0	402,793.0	519.2	49.2	0.05	0.07	8.8	0.085	0.06
KNRC002	28	29	5,425,899.0	402,793.0	518.2	48.3	0.04	0.11	8.7	0.11	0.19
KNRC002	29	30	5,425,899.0	402,793.0	517.2	50.2	0.04	0.08	7.9	0.061	0.42
KNRC002	30	31	5,425,899.0	402,793.0	516.2	41.7	0.07	0.06	11.1	0.093	0.18
KNRC002	31	32	5,425,899.0	402,793.0	515.2	47.7	0.05	0.06	8.6	0.044	0.78
KNRC002	32	33	5,425,899.0	402,793.0	514.2	39.7	0.03	0.05	12.2	0.038	0.89
KNRC002	33	34	5,425,899.0	402,793.0	513.2	43.1	0.06	0.07	11.8	0.028	0.16
KNRC002	34	35	5,425,899.0	402,793.0	512.2	38.3	0.02	0.07	12.3	0.039	0.3
KNRC002	35	36	5,425,899.0	402,793.0	511.2	35.8	0.05	0.06	15.6	0.068	0.35
KNRC002	36	37	5,425,899.0	402,793.0	510.2	35.9	0.04	0.06	16.8	0.064	0.28
KNRC002	37	38	5,425,899.0	402,793.0	509.2	23.7	0.03	0.03	11.1	0.037	0.18
KNRC002	38	39	5,425,899.0	402,793.0	508.2	43.1	0.03	0.05	9.2	0.074	0.6
KNRC002	39	40	5,425,899.0	402,793.0	507.2	43.9	0.04	0.05	9.3	0.082	0.59
KNRC002	40	41	5,425,899.0	402,793.0	506.2	40.2	0.03	0.05	10	0.068	0.41
KNRC002	41	42	5,425,899.0	402,793.0	505.2	50	0.02	0.05	7.2	0.076	0.17
KNRC002	42	43	5,425,899.0	402,793.0	504.2	36.3	0.02	0.04	7.6	0.11	0.36
KNRC003	7	8	5,425,902.0	402,761.0	539.4	46.8	0.08	0.08	5.6	0.025	0.11
KNRC003	8	9	5,425,902.0	402,761.0	538.4	12.6	0.05	0.05	3.5	0.024	0.1
KNRC003	9	10	5,425,902.0	402,761.0	537.4	24.9	0.07	0.05	6.6	0.041	0.09
KNRC003	10	11	5,425,902.0	402,761.0	536.4	20.5	0.13	0.05	12.2	0.034	0.07
KNRC003	11	12	5,425,902.0	402,761.0	535.4	33.8	0.07	0.06	7.2	0.038	0.09
KNRC003	12	13	5,425,902.0	402,761.0	534.4	46.8	0.09	0.07	5.6	0.042	2.4
KNRC003	13	14	5,425,902.0	402,761.0	533.4	43.9	0.01	0.04	4.5	0.028	2.9
KNRC003	14	15	5,425,902.0	402,761.0	532.4	31.1	0.07	0.04	8.2	0.095	0.54
KNRC003	15	16	5,425,902.0	402,761.0	531.4	45.8	0.08	0.07	7.9	0.17	1.8
KNRC003	16	17	5,425,902.0	402,761.0	530.4	25.5	0.16	0.04	22.6	0.19	0.25
KNRC003	17	18	5,425,902.0	402,761.0	529.4	24.1	0.14	0.03	23.4	0.19	0.23
KNRC003	18	19	5,425,902.0	402,761.0	528.4	23	0.15	0.03	22.3	0.14	0.43
KNRC003	19	20	5,425,902.0	402,761.0	527.4	29.4	0.14	0.04	16.8	0.058	0.33
KNRC003	20	21	5,425,902.0	402,761.0	526.4	26.3	0.14	0.05	18	0.025	0.7
KNRC003	21	22	5,425,902.0	402,761.0	525.4	20.5	0.13	0.02	24.2	0.024	0.93
KNRC003	22	23	5,425,902.0	402,761.0	524.4	27.7	0.18	0.02	21.1	0.023	1.5
KNRC003	23	24	5,425,902.0	402,761.0	523.4	25.2	0.18	0.03	19.3	0.021	2.9
KNRC003	24	25	5,425,902.0	402,761.0	522.4	23.9	0.16	0.03	21.2	0.016	2.3
KNRC003	25	26	5,425,902.0	402,761.0	521.4	24.6	0.11	0.02	20.1	0.057	1.3
KNRC003	26	27	5,425,902.0	402,761.0	520.4	23.7	0.05	0.02	18.4	0.076	4.6
KNRC003	27	28	5,425,902.0	402,761.0	519.4	19.6	0.08	0.01	21.4	0.25	3.7
KNRC003	28	29	5,425,902.0	402,761.0	518.4	21.1	0.08	0.01	21.3	0.084	2
KNRC003	29	30	5,425,902.0	402,761.0	517.4	18.4	0.1	0.02	24.6	0.047	2.1
KNRC003	30	31	5,425,902.0	402,761.0	516.4	19.5	0.03		22.9	0.037	3.5
KNRC003	31	32	5,425,902.0	402,761.0	515.4	25.8	0.11	0.02	19	0.049	3.6
KNRC003	32	33	5,425,902.0	402,761.0	514.4	24.4	0.1	0.02	21.5	0.028	1.8
KNRC003	33	34	5,425,902.0	402,761.0	513.4	40	0.07	0.04	12.9	0.028	2.3
KNRC003	34	35	5,425,902.0	402,761.0	512.4	22.2	0.05	0.02	19.9	0.042	1.4
KNRC003	35	36	5,425,902.0	402,761.0	511.4	26.5	0.05	0.03	20	0.018	1.9
KNRC007	1	2	5,425,798.0	402,760.0	547.4	61.6	0.06	0.15	0.33	0.032	0.08
KNRC007	2	3	5,425,798.0	402,760.0	546.4	60.5	0.07	0.15	0.15	0.021	0.06

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC007	3	4	5,425,798.0	402,760.0	545.4	60.1	0.05	0.15	0.31	0.02	0.04
KNRC007	4	5	5,425,798.0	402,760.0	544.4	57.4	0.06	0.17	0.25	0.029	0.05
KNRC007	5	6	5,425,798.0	402,760.0	543.4	55.8	0.05	0.16	1.4	0.026	0.04
KNRC007	6	7	5,425,798.0	402,760.0	542.4	58.7	0.05	0.16	1	0.025	0.04
KNRC007	7	8	5,425,798.0	402,760.0	541.4	49.3	0.06	0.14	3.6	0.026	0.13
KNRC007	8	9	5,425,798.0	402,760.0	540.4	57.1	0.04	0.16	1.9	0.028	0.04
KNRC007	9	10	5,425,798.0	402,760.0	539.4	61.1	0.04	0.16	1	0.027	0.02
KNRC007	10	11	5,425,798.0	402,760.0	538.4	58	0.06	0.17	3.7	0.048	0.03
KNRC007	11	12	5,425,798.0	402,760.0	537.4	49.8	0.05	0.14	7.2	0.06	0.01
KNRC007	12	13	5,425,798.0	402,760.0	536.4	55.6	0.06	0.16	5.8	0.062	
KNRC007	13	14	5,425,798.0	402,760.0	535.4	57.5	0.03	0.17	3.3	0.03	0.01
KNRC007	14	15	5,425,798.0	402,760.0	534.4	52.6	0.04	0.18	4.4	0.034	
KNRC007	15	16	5,425,798.0	402,760.0	533.4	57.6	0.03	0.21	2.6	0.029	
KNRC007	16	17	5,425,798.0	402,760.0	532.4	57.1	0.04	0.22	3.1	0.025	
KNRC007	17	18	5,425,798.0	402,760.0	531.4	56.3	0.04	0.11	5.4	0.041	
KNRC007	18	19	5,425,798.0	402,760.0	530.4	53.3	0.07	0.13	8	0.03	
KNRC007	19	20	5,425,798.0	402,760.0	529.4	49.7	0.11	0.11	10.3	0.013	
KNRC007	20	21	5,425,798.0	402,760.0	528.4	61.5	0.04	0.17	3.3	0.009	0.01
KNRC007	21	22	5,425,798.0	402,760.0	527.4	61.4	0.03	0.2	2.6	0.011	
KNRC007	22	23	5,425,798.0	402,760.0	526.4	54.2	0.05	0.19	5.1	0.052	0.02
KNRC007	23	24	5,425,798.0	402,760.0	525.4	58.9	0.04	0.22	2.2	0.023	0.01
KNRC007	24	25	5,425,798.0	402,760.0	524.4	54.7	0.06	0.19	6.3	0.015	
KNRC007	25	26	5,425,798.0	402,760.0	523.4	56.6	0.04	0.18	5.2	0.015	
KNRC007	26	27	5,425,798.0	402,760.0	522.4	61.7	0.04	0.17	2.2	0.009	
KNRC007	27	28	5,425,798.0	402,760.0	521.4	58.9	0.02	0.16	3.9	0.01	
KNRC007	28	29	5,425,798.0	402,760.0	520.4	40.3	0.07	0.11	14.4	0.011	0.01
KNRC007	29	30	5,425,798.0	402,760.0	519.4	38.9	0.05	0.09	14.9	0.074	
KNRC007	30	31	5,425,798.0	402,760.0	518.4	54.5	0.07	0.13	7.9		0.01
KNRC007	31	32	5,425,798.0	402,760.0	517.4	57.6	0.04	0.15	6.2	0.009	
KNRC007	32	33	5,425,798.0	402,760.0	516.4	42.6	0.03	0.12	14.4	0.014	
KNRC007	33	34	5,425,798.0	402,760.0	515.4	33.5	0.04	0.08	19.1		
KNRC007	34	35	5,425,798.0	402,760.0	514.4	57.9	0.02	0.16	5.7	0.008	0.02
KNRC007	35	36	5,425,798.0	402,760.0	513.4	59.2	0.02	0.14	5.1	0.005	
KNRC007	36	37	5,425,798.0	402,760.0	512.4	57.4	0.03	0.14	5.5	0.005	
KNRC007	37	38	5,425,798.0	402,760.0	511.4	34.7	0.05	0.08	20.3	0.011	0.05
KNRC007	38	39	5,425,798.0	402,760.0	510.4	52.3	0.03	0.13	8.1	0.01	0.02
KNRC007	39	40	5,425,798.0	402,760.0	509.4	44	0.03	0.13	7.4	0.038	0.09
KNRC007	40	41	5,425,798.0	402,760.0	508.4	26.6	0.1	0.03	25.9	0.19	0.01
KNRC007	41	42	5,425,798.0	402,760.0	507.4	29.7	0.08	0.05	19.7	0.041	0.08
KNRC008	20	21	5,425,798.0	402,720.0	527.3	26.6	0.09	0.23	16.8	0.033	
KNRC008	21	22	5,425,798.0	402,720.0	526.3	46.1	0.05	0.26	9	0.023	0.03
KNRC008	22	23	5,425,798.0	402,720.0	525.3	32.9	0.05	0.21	20.1	0.023	0.01
KNRC008	23	24	5,425,798.0	402,720.0	524.3	46.4	0.04	0.23	10.1	0.012	0.03
KNRC008	24	25	5,425,798.0	402,720.0	523.3	35.6	0.02	0.41	12.9	0.061	0.2
KNRC008	25	26	5,425,798.0	402,720.0	522.3	29.4	0.03	0.36	17.9	0.018	0.19
KNRC008	26	27	5,425,798.0	402,720.0	521.3	35.4	0.03	0.25	13.7	0.026	0.09
KNRC008	27	28	5,425,798.0	402,720.0	520.3	47.5	0.02	0.25	8	0.015	0.11
KNRC008	28	29	5,425,798.0	402,720.0	519.3	43.3	0.06	0.26	11	0.014	0.1
KNRC008	29	30	5,425,798.0	402,720.0	518.3	23.6	0.06	0.3	17.8	0.15	0.26

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC008	30	31	5,425,798.0	402,720.0	517.3	25.1	0.01	0.1	20.9	0.18	0.03
KNRC008	31	32	5,425,798.0	402,720.0	516.3	23.5	0.02	0.08	22.1	0.14	0.02
KNRC008	32	33	5,425,798.0	402,720.0	515.3	32.5		0.11	17.4	0.04	0.02
KNRC008	33	34	5,425,798.0	402,720.0	514.3	33.7	0.02	0.1	15.6	0.056	0.02
KNRC008	34	35	5,425,798.0	402,720.0	513.3	32.4	0.01	0.12	12.6	0.059	0.31
KNRC008	35	36	5,425,798.0	402,720.0	512.3	30.6	0.03	0.12	11.3	0.063	0.16
KNRC008	36	37	5,425,798.0	402,720.0	511.3	31.6	0.02	0.11	14	0.065	0.04
KNRC008	37	38	5,425,798.0	402,720.0	510.3	26.6	0.04	0.11	16.7	0.04	0.05
KNRC008	38	39	5,425,798.0	402,720.0	509.3	33.5	0.01	0.12	10.3	0.039	0.91
KNRC008	39	40	5,425,798.0	402,720.0	508.3	34.5	0.04	0.11	6.2	0.097	3.5
KNRC008	40	41	5,425,798.0	402,720.0	507.3	28.6	0.02	0.1	11.6	0.069	1.5
KNRC008	41	42	5,425,798.0	402,720.0	506.3	19.6	0.01	0.09	10	0.053	2.3
KNRC008	42	43	5,425,798.0	402,720.0	505.3	29.9	0.02	0.1	7.4	0.049	4.3
KNRC008	43	44	5,425,798.0	402,720.0	504.3	32.8	0.05	0.1	7.7	0.044	8.1
KNRC008	44	45	5,425,798.0	402,720.0	503.3	37.1	0.03	0.11	5	0.06	7.9
KNRC008	45	46	5,425,798.0	402,720.0	502.3	31.5	0.07	0.1	5.7	0.063	11.5
KNRC008	46	47	5,425,798.0	402,720.0	501.3	28.9	0.08	0.11	11.8	0.083	14.7
KNRC008	47	48	5,425,798.0	402,720.0	500.3	31.7	0.16	0.07	11.5	0.015	12.7
KNRC008	48	49	5,425,798.0	402,720.0	499.3	26.3	0.19	0.04	13.4	0.044	19.6
KNRC008	63	64	5,425,798.0	402,720.0	484.3	19.3	0.22		29.8	0.015	0.37
KNRC008	64	65	5,425,798.0	402,720.0	483.3	25.3	0.18	0.04	26.2	0.014	0.28
KNRC008	65	66	5,425,798.0	402,720.0	482.3	39.4	0.09	0.09	15.2	0.021	0.17
KNRC008	66	67	5,425,798.0	402,720.0	481.3	27.4	0.17	0.05	23.5	0.02	0.94
KNRC008	67	68	5,425,798.0	402,720.0	480.3	29.3	0.08	0.08	15.6	0.049	0.56
KNRC008	68	69	5,425,798.0	402,720.0	479.3	24.4	0.06	0.13	14.1	0.081	1.6
KNRC008	69	70	5,425,798.0	402,720.0	478.3	26.7	0.08	0.09	14.5	0.073	0.9
KNRC008	70	71	5,425,798.0	402,720.0	477.3	27.7	0.06	0.09	13.5	0.088	0.85
KNRC008	71	72	5,425,798.0	402,720.0	476.3	25.6	0.05	0.07	13.5	0.12	0.08
KNRC008	72	73	5,425,798.0	402,720.0	475.3	38.1	0.05	0.06	10.6	0.13	0.33
KNRC008	73	74	5,425,798.0	402,720.0	474.3	41	0.05	0.06	11.8	0.12	0.73
KNRC008	74	75	5,425,798.0	402,720.0	473.3	41.1	0.07	0.07	14.5	0.062	0.08
KNRC008	75	76	5,425,798.0	402,720.0	472.3	35.9	0.1	0.06	17.3	0.05	0.07
KNRC008	76	77	5,425,798.0	402,720.0	471.3	34.1	0.1	0.05	18.6	0.057	0.03
KNRC008	77	78	5,425,798.0	402,720.0	470.3	42	0.09	0.06	15	0.029	0.02
KNRC008	78	79	5,425,798.0	402,720.0	469.3	33.6	0.11	0.04	19.8	0.036	0.03
KNRC008	79	80	5,425,798.0	402,720.0	468.3	36.8	0.11	0.04	18.3	0.039	0.03
KNRC008	80	81	5,425,798.0	402,720.0	467.3	35.7	0.09	0.03	17.3	0.044	0.05
KNRC008	81	82	5,425,798.0	402,720.0	466.3	27.7	0.11	0.02	23.1	0.06	0.09
KNRC008	82	83	5,425,798.0	402,720.0	465.3	22.6	0.1	0.02	26.2	0.069	0.05
KNRC008	83	84	5,425,798.0	402,720.0	464.3	26.2	0.13	0.03	24.3	0.12	0.03
KNRC008	84	85	5,425,798.0	402,720.0	463.3	22.9	0.08	0.03	21.6	0.09	0.08
KNRC008	85	86	5,425,798.0	402,720.0	462.3	27.7	0.06	0.07	13.5	0.052	0.2
KNRC008	86	87	5,425,798.0	402,720.0	461.3	47.3	0.06	0.09	7.1	0.022	0.2
KNRC008	87	88	5,425,798.0	402,720.0	460.3	27.5	0.09	0.03	18.9	0.03	0.18
KNRC008	88	89	5,425,798.0	402,720.0	459.3	30	0.07	0.04	15	0.027	0.12
KNRC008	89	90	5,425,798.0	402,720.0	458.3	43	0.06	0.06	8.6	0.018	1.1
KNRC014	28	29	5,425,727.0	402,731.0	519.5	38.2	0.06	0.18	12.1	0.029	
KNRC014	29	30	5,425,727.0	402,731.0	518.5	34.6	0.08	0.14	15	0.025	
KNRC014	30	31	5,425,727.0	402,731.0	517.5	21	0.1	0.17	20.7	0.049	

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC014	31	32	5,425,727.0	402,731.0	516.5	27	0.1	0.15	15.6	0.052	
KNRC014	32	33	5,425,727.0	402,731.0	515.5	23.1	0.13	0.13	16.4	0.036	
KNRC014	33	34	5,425,727.0	402,731.0	514.5	22.2	0.08	0.13	18.1	0.049	
KNRC014	34	35	5,425,727.0	402,731.0	513.5	47.3	0.07	0.14	8.5	0.019	
KNRC014	35	36	5,425,727.0	402,731.0	512.5	46.5	0.06	0.14	7.6	0.025	
KNRC014	36	37	5,425,727.0	402,731.0	511.5	41	0.03	0.17	8.3	0.029	
KNRC014	42	43	5,425,727.0	402,731.0	505.5	53.9	0.05	0.17	7.2	0.029	
KNRC014	43	44	5,425,727.0	402,731.0	504.5	26.6	0.01	0.06	21.6	0.042	
KNRC014	44	45	5,425,727.0	402,731.0	503.5	39.7	0.01	0.09	13.7	0.052	
KNRC014	45	46	5,425,727.0	402,731.0	502.5	51.1	0.03	0.13	10.1	0.067	
KNRC014	46	47	5,425,727.0	402,731.0	501.5	49.2	0.06	0.1	11.7	0.047	0.03
KNRC014	47	48	5,425,727.0	402,731.0	500.5	34.1	0.04	0.05	16.2	0.042	0.16
KNRC014	48	49	5,425,727.0	402,731.0	499.5	35.4	0.03	0.06	14.3	0.034	0.08
KNRC014	49	50	5,425,727.0	402,731.0	498.5	41.4	0.05	0.06	13.3	0.052	0.03
KNRC014	50	51	5,425,727.0	402,731.0	497.5	37.4	0.03	0.05	11.6	0.055	0.04
KNRC014	51	52	5,425,727.0	402,731.0	496.5	40.4	0.03	0.05	11.3	0.049	
KNRC014	52	53	5,425,727.0	402,731.0	495.5	35.2	0.05	0.04	13.3	0.039	
KNRC014	53	54	5,425,727.0	402,731.0	494.5	18	0.08	0.02	43	0.031	
KNRC014	54	55	5,425,727.0	402,731.0	493.5	32.4	0.05	0.04	22.6	0.042	
KNRC014	55	56	5,425,727.0	402,731.0	492.5	35.4	0.02	0.06	15.5	0.027	0.01
KNRC014	56	57	5,425,727.0	402,731.0	491.5	25.7	0.04	0.03	20	0.012	
KNRC015	8	9	5,425,732.0	402,769.0	539.2	39.6	0.15	0.09	5.7	0.027	0.07
KNRC015	9	10	5,425,732.0	402,769.0	538.2	63	0.02	0.12	0.89	0.01	0.04
KNRC015	10	11	5,425,732.0	402,769.0	537.2	63.9	0.04	0.12	0.58	0.008	0.03
KNRC015	11	12	5,425,732.0	402,769.0	536.2	61.1	0.06	0.13	2.6	0.009	0.02
KNRC015	12	13	5,425,732.0	402,769.0	535.2	61.2	0.07	0.12	1.5	0.011	0.03
KNRC015	13	14	5,425,732.0	402,769.0	534.2	58.8	0.07	0.11	2	0.01	0.03
KNRC015	14	15	5,425,732.0	402,769.0	533.2	55.7	0.07	0.11	3.4	0.015	0.02
KNRC015	15	16	5,425,732.0	402,769.0	532.2	34.5	0.04	0.09	5.5	0.03	0.02
KNRC015	16	17	5,425,732.0	402,769.0	531.2	42.5	0.1	0.1	14.5	0.012	
KNRC015	17	18	5,425,732.0	402,769.0	530.2	39.9	0.15	0.08	17	0.008	
KNRC015	18	19	5,425,732.0	402,769.0	529.2	45.6	0.17	0.09	14.1	0.004	
KNRC015	19	20	5,425,732.0	402,769.0	528.2	27.3	0.16	0.03	24.3	0.006	
KNRC016	2	3	5,425,720.0	402,818.0	544.1	44.6	0.04	0.15	2.7	0.081	0.01
KNRC016	3	4	5,425,720.0	402,818.0	543.1	46.6	0.04	0.17	2.3	0.083	0.04
KNRC016	4	5	5,425,720.0	402,818.0	542.1	47.3	0.05	0.16	2.4	0.078	0.03
KNRC016	5	6	5,425,720.0	402,818.0	541.1	52.4	0.04	0.17	4.3	0.072	0.01
KNRC016	6	7	5,425,720.0	402,818.0	540.1	50.4	0.04	0.18	5.2	0.056	
KNRC016	7	8	5,425,720.0	402,818.0	539.1	49.6	0.04	0.17	5.3	0.052	0.01
KNRC017	59	60	5,425,654.0	402,707.0	487.4	23.9	0.11	0.05	27.8	0.093	
KNRC017	60	61	5,425,654.0	402,707.0	486.4	22.8	0.1	0.05	28.7	0.071	0.02
KNRC017	61	62	5,425,654.0	402,707.0	485.4	24	0.11	0.05	27.5	0.072	
KNRC017	62	63	5,425,654.0	402,707.0	484.4	26.4	0.12	0.05	26.4	0.036	
KNRC017	63	64	5,425,654.0	402,707.0	483.4	24.4	0.1	0.05	27.3	0.034	
KNRC017	64	65	5,425,654.0	402,707.0	482.4	24.6	0.12	0.05	28.1	0.017	
KNRC017	65	66	5,425,654.0	402,707.0	481.4	27.4	0.09	0.06	25.2	0.025	
KNRC017	66	67	5,425,654.0	402,707.0	480.4	27.8	0.1	0.05	24.1	0.042	
KNRC017	67	68	5,425,654.0	402,707.0	479.4	27.3	0.14	0.05	22.7	0.056	
KNRC017	68	69	5,425,654.0	402,707.0	478.4	24.8	0.12	0.05	23.7	0.014	

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC017	69	70	5,425,654.0	402,707.0	477.4	30.5	0.08	0.06	22.1	0.02	
KNRC017	70	71	5,425,654.0	402,707.0	476.4	39.9	0.05	0.09	17.5	0.015	
KNRC018	37	38	5,425,664.0	402,742.0	509.8	28.6	0.06	0.05	20.4	0.025	0.02
KNRC018	38	39	5,425,664.0	402,742.0	508.8	47.5	0.05	0.1	8.6	0.027	
KNRC018	39	40	5,425,664.0	402,742.0	507.8	45.3	0.02	0.1	12.3	0.032	
KNRC018	40	41	5,425,664.0	402,742.0	506.8	28.5	0.05	0.05	21.9	0.079	0.04
KNRC018	41	42	5,425,664.0	402,742.0	505.8	27.9	0.04	0.05	22.1	0.022	
KNRC018	42	43	5,425,664.0	402,742.0	504.8	34.8	0.06	0.04	19.8	0.046	
KNRC018	43	44	5,425,664.0	402,742.0	503.8	30.4		0.05	21.1	0.067	
KNRC018	44	45	5,425,664.0	402,742.0	502.8	31.4	0.13	0.06	23.3	0.027	
KNRC018	45	46	5,425,664.0	402,742.0	501.8	40.7	0.11	0.1	18.3	0.011	
KNRC018	46	47	5,425,664.0	402,742.0	500.8	27.8	0.09	0.04	23.8	0.014	
KNRC019	16	17	5,425,671.0	402,786.0	530.0	27.2	0.16	0.05	25.2	0.042	0.33
KNRC019	17	18	5,425,671.0	402,786.0	529.0	27.2	0.13	0.06	21.9	0.11	0.04
KNRC019	18	19	5,425,671.0	402,786.0	528.0	40.6	0.06	0.12	10.6	0.053	0.02
KNRC019	19	20	5,425,671.0	402,786.0	527.0	28.5	0.06	0.07	20.6	0.11	0.02
KNRC019	20	21	5,425,671.0	402,786.0	526.0	34.6	0.02	0.09	14.8	0.11	0.02
KNRC019	21	22	5,425,671.0	402,786.0	525.0	31.5	0.06	0.08	17.9	0.064	0.02
KNRC019	22	23	5,425,671.0	402,786.0	524.0	25.9	0.12	0.07	23	0.051	0.01
KNRC019	23	24	5,425,671.0	402,786.0	523.0	25.6	0.06	0.08	19.9	0.066	0.03
KNRC020	13	14	5,425,654.0	402,819.0	531.8	41.5	0.04	0.07	14.8	0.044	
KNRC020	14	15	5,425,654.0	402,819.0	530.8	36.4	0.04	0.05	15.3	0.048	
KNRC020	15	16	5,425,654.0	402,819.0	529.8	21.2	0.07	0.03	26.7	0.13	
KNRC020	16	17	5,425,654.0	402,819.0	528.8	22.7	0.05	0.04	23.1	0.047	
KNRC020	17	18	5,425,654.0	402,819.0	527.8	21.3	0.04	0.03	24.4	0.052	
KNRC020	18	19	5,425,654.0	402,819.0	526.8	28.3	0.03	0.04	20.7	0.074	
KNRC020	19	20	5,425,654.0	402,819.0	525.8	24.3	0.01	0.03	20.5	0.085	
KNRC020	20	21	5,425,654.0	402,819.0	524.8	23.5	0.05	0.02	25.3	0.047	
KNRC020	21	22	5,425,654.0	402,819.0	523.8	35.6	0.07	0.06	20	0.04	
KNRC020	22	23	5,425,654.0	402,819.0	522.8	38.7	0.03	0.08	15.4	0.025	
KNRC020	23	24	5,425,654.0	402,819.0	521.8	23.8	0.04	0.03	24.9	0.049	
KNRC020	24	25	5,425,654.0	402,819.0	520.8	33.9	0.04	0.04	18.6	0.018	0.05
KNRC020	25	26	5,425,654.0	402,819.0	519.8	32.5	0.03	0.03	20.2	0.045	
KNRC020	26	27	5,425,654.0	402,819.0	518.8	40.1	0.04	0.05	16.2	0.063	0.01
KNRC020	27	28	5,425,654.0	402,819.0	517.8	36.4	0.05	0.05	19	0.044	
KNRC020	28	29	5,425,654.0	402,819.0	516.8	24.8	0.06	0.02	25.2	0.041	
KNRC020	29	30	5,425,654.0	402,819.0	515.8	24.6	0.03	0.02	23.2	0.04	
KNRC020	30	31	5,425,654.0	402,819.0	514.8	15.9		0.03	23.5	0.015	0.01
KNRC020	31	32	5,425,654.0	402,819.0	513.8	21		0.03	21.1	0.045	
KNRC020	32	33	5,425,654.0	402,819.0	512.8	31.2		0.03	18.6	0.03	
KNRC020B	2.37	3.37	5,425,616.0	402,850.0	539.9	45.922	0.0978	0.08	9.104	0.0626	0.0163
KNRC020B	3.37	4.37	5,425,616.0	402,850.0	538.9	43.377	0.0711	0.0689	11.782	0.0502	0.01
KNRC020B	4.37	5.37	5,425,616.0	402,850.0	537.9	31.7818	0.0718	0.0645	14.6182	0.0376	0.02
KNRC021	17	18	5,425,582.0	402,580.0	525.0	30.7	0.2	0.09	19.5	0.058	
KNRC021	18	19	5,425,582.0	402,580.0	524.0	36.5	0.11	0.12	12.6	0.12	0.03
KNRC021	19	20	5,425,582.0	402,580.0	523.0	57.5	0.03	0.16	2.6	0.084	
KNRC021	20	21	5,425,582.0	402,580.0	522.0	51.3	0.06	0.14	6.3	0.093	0.01
KNRC021	21	22	5,425,582.0	402,580.0	521.0	40	0.06	0.09	13.2	0.094	0.02
KNRC021	22	23	5,425,582.0	402,580.0	520.0	34.1	0.05	0.07	17.1	0.086	

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC021	23	24	5,425,582.0	402,580.0	519.0	40	0.02	0.1	12.8	0.047	0.02
KNRC021	24	25	5,425,582.0	402,580.0	518.0	27.5	0.19	0.05	24.5	0.038	
KNRC021	25	26	5,425,582.0	402,580.0	517.0	37.9	0.09	0.12	14.9	0.086	
KNRC021	26	27	5,425,582.0	402,580.0	516.0	36.5	0.06	0.1	14.4	0.086	
KNRC021	27	28	5,425,582.0	402,580.0	515.0	33.7	0.04	0.06	16.2	0.07	
KNRC021	28	29	5,425,582.0	402,580.0	514.0	29.4	0.08	0.06	18	0.06	0.03
KNRC021	29	30	5,425,582.0	402,580.0	513.0	26	0.14	0.04	22.9	0.032	
KNRC021	30	31	5,425,582.0	402,580.0	512.0	30.1	0.16	0.04	19.9	0.059	
KNRC021	63	64	5,425,582.0	402,580.0	479.0	24.8	0.19	0.06	25	0.11	0.01
KNRC021	64	65	5,425,582.0	402,580.0	478.0	30.2	0.23	0.07	21.1	0.16	
KNRC021	65	66	5,425,582.0	402,580.0	477.0	38.7	0.16	0.1	14.4	0.14	0.01
KNRC021	66	67	5,425,582.0	402,580.0	476.0	22.2	0.76	0.06	24	0.063	
KNRC021	67	68	5,425,582.0	402,580.0	475.0	35.8	0.15	0.09	12.6	0.078	
KNRC021	68	69	5,425,582.0	402,580.0	474.0	27.8	0.11	0.04	23	0.032	
KNRC021	69	70	5,425,582.0	402,580.0	473.0	38.3	0.16	0.07	15	0.12	0.01
KNRC021	70	71	5,425,582.0	402,580.0	472.0	29.5	0.09	0.06	19	0.039	0.02
KNRC023	22	23	5,425,582.0	402,660.0	521.3	42	0.11	0.11	13.7	0.021	0.02
KNRC023	23	24	5,425,582.0	402,660.0	520.3	12.1	0.05	0.06	11	0.038	0.01
KNRC023	24	25	5,425,582.0	402,660.0	519.3	33.2	0.09	0.1	16.2	0.028	0.31
KNRC023	25	26	5,425,582.0	402,660.0	518.3	51.1	0.03	0.09	8.2	0.013	0.02
KNRC023	26	27	5,425,582.0	402,660.0	517.3	22.3	0.05	0.17	15	0.2	0.04
KNRC023	27	28	5,425,582.0	402,660.0	516.3	48.5	0.03	0.1	9.9	0.02	0.02
KNRC023	28	29	5,425,582.0	402,660.0	515.3	38.5	0.07	0.1	14.5	0.032	0.14
KNRC023	29	30	5,425,582.0	402,660.0	514.3	36.4	0.06	0.08	15.5	0.052	0.05
KNRC023	30	31	5,425,582.0	402,660.0	513.3	36.4	0.05	0.1	14.7	0.088	0.03
KNRC023	31	32	5,425,582.0	402,660.0	512.3	46.9	0.06	0.09	12.5	0.025	0.02
KNRC023	32	33	5,425,582.0	402,660.0	511.3	23.2	0.13	0.03	27.2	0.021	0.01
KNRC023	33	34	5,425,582.0	402,660.0	510.3	22.5	0.14	0.04	25.6	0.031	
KNRC023	34	35	5,425,582.0	402,660.0	509.3	25.4	0.14	0.04	25.5	0.024	
KNRC023	40	41	5,425,582.0	402,660.0	503.3	26.8	0.1	0.04	22.2	0.022	0.02
KNRC023	41	42	5,425,582.0	402,660.0	502.3	23.8	0.08	0.05	18.9	0.04	0.03
KNRC023	42	43	5,425,582.0	402,660.0	501.3	30.2	0.09	0.08	13.8	0.011	0.04
KNRC023	43	44	5,425,582.0	402,660.0	500.3	38.3	0.13	0.08	11.2	0.019	0.05
KNRC023	46	47	5,425,582.0	402,660.0	497.3	18.9	0.05	0.15	19.7	0.044	0.37
KNRC023	47	48	5,425,582.0	402,660.0	496.3	16.4	0.04	0.23	20.7	0.021	0.23
KNRC023	48	49	5,425,582.0	402,660.0	495.3	28.6	0.08	0.05	17.3	0.021	0.04
KNRC023	49	50	5,425,582.0	402,660.0	494.3	22.3	0.08	0.04	21.9	0.044	0.03
KNRC023	50	51	5,425,582.0	402,660.0	493.3	28.5	0.09	0.04	19.1	0.02	0.03
KNRC023	51	52	5,425,582.0	402,660.0	492.3	37.5	0.06	0.08	12.2	0.016	0.04
KNRC023	52	53	5,425,582.0	402,660.0	491.3	34	0.04	0.1	11	0.047	0.02
KNRC023	53	54	5,425,582.0	402,660.0	490.3	40.3	0.02	0.13	8.5	0.041	0.02
KNRC023	54	55	5,425,582.0	402,660.0	489.3	47.2	0.03	0.11	8.1	0.024	0.02
KNRC023	55	56	5,425,582.0	402,660.0	488.3	36.1	0.06	0.09	12	0.028	0.02
KNRC023	56	57	5,425,582.0	402,660.0	487.3	36.9	0.04	0.11	18.2	0.033	
KNRC023	57	58	5,425,582.0	402,660.0	486.3	39.2	0.03	0.11	16.2	0.023	0.02
KNRC023	58	59	5,425,582.0	402,660.0	485.3	43.8	0.03	0.12	12.9	0.018	
KNRC023	59	60	5,425,582.0	402,660.0	484.3	18.8	0.07	0.05	27	0.035	0.01
KNRC023	60	61	5,425,582.0	402,660.0	483.3	25.9	0.05	0.06	22.6	0.048	
KNRC023	61	62	5,425,582.0	402,660.0	482.3	52	0.01	0.15	8.6	0.026	0.01

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC023	62	63	5,425,582.0	402,660.0	481.3	13.6	0.05	0.02	32.7	0.025	
KNRC023	63	64	5,425,582.0	402,660.0	480.3	22.9	0.14	0.03	24.3	0.022	
KNRC023	64	65	5,425,582.0	402,660.0	479.3	34.6	0.09	0.07	13.2	0.036	0.02
KNRC023	65	66	5,425,582.0	402,660.0	478.3	34.6	0.11	0.07	13.6	0.02	0.01
KNRC023	22	23	5,425,582.0	402,660.0	521.3	42	0.11	0.11	13.7	0.021	0.02
KNRC023	23	24	5,425,582.0	402,660.0	520.3	12.1	0.05	0.06	11	0.038	0.01
KNRC023	24	25	5,425,582.0	402,660.0	519.3	33.2	0.09	0.1	16.2	0.028	0.31
KNRC023	25	26	5,425,582.0	402,660.0	518.3	51.1	0.03	0.09	8.2	0.013	0.02
KNRC023	26	27	5,425,582.0	402,660.0	517.3	22.3	0.05	0.17	15	0.2	0.04
KNRC023	27	28	5,425,582.0	402,660.0	516.3	48.5	0.03	0.1	9.9	0.02	0.02
KNRC023	28	29	5,425,582.0	402,660.0	515.3	38.5	0.07	0.1	14.5	0.032	0.14
KNRC023	29	30	5,425,582.0	402,660.0	514.3	36.4	0.06	0.08	15.5	0.052	0.05
KNRC023	30	31	5,425,582.0	402,660.0	513.3	36.4	0.05	0.1	14.7	0.088	0.03
KNRC023	31	32	5,425,582.0	402,660.0	512.3	46.9	0.06	0.09	12.5	0.025	0.02
KNRC023	32	33	5,425,582.0	402,660.0	511.3	23.2	0.13	0.03	27.2	0.021	0.01
KNRC023	33	34	5,425,582.0	402,660.0	510.3	22.5	0.14	0.04	25.6	0.031	
KNRC023	34	35	5,425,582.0	402,660.0	509.3	25.4	0.14	0.04	25.5	0.024	
KNRC026	20	21	5,425,582.0	402,781.0	523.1	32.7	0.02	0.08	17.6	0.022	0.04
KNRC026	21	22	5,425,582.0	402,781.0	522.1	47.1	0.02	0.11	11	0.006	0.03
KNRC026	22	23	5,425,582.0	402,781.0	521.1	39.6	0.02	0.09	15.1	0.02	0.04
KNRC026	23	24	5,425,582.0	402,781.0	520.1	43.8	0.02	0.1	12.9	0.015	0.03
KNRC026	24	25	5,425,582.0	402,781.0	519.1	39	0.01	0.08	15.3	0.011	0.1
KNRC026	25	26	5,425,582.0	402,781.0	518.1	30	0.01	0.07	20.7	0.031	0.19
KNRC026	26	27	5,425,582.0	402,781.0	517.1	40.2	0.01	0.09	13.5	0.015	0.02
KNRC026	27	28	5,425,582.0	402,781.0	516.1	36.4	0.01	0.09	16.9	0.018	
KNRC026	28	29	5,425,582.0	402,781.0	515.1	56.1	0.02	0.13	6.9	0.009	
KNRC026	29	30	5,425,582.0	402,781.0	514.1	45.6	0.03	0.11	12.9	0.013	
KNRC026	30	31	5,425,582.0	402,781.0	513.1	49.3	0.02	0.13	10.6	0.007	
KNRC026	31	32	5,425,582.0	402,781.0	512.1	51.9	0.01	0.13	9.5	0.009	0.02
KNRC026	32	33	5,425,582.0	402,781.0	511.1	43.7		0.11	12.6	0.004	
KNRC026	33	34	5,425,582.0	402,781.0	510.1	43.2	0.01	0.12	12.9	0.006	
KNRC026	34	35	5,425,582.0	402,781.0	509.1	41.1	0.02	0.1	15	0.008	0.01
KNRC026	35	36	5,425,582.0	402,781.0	508.1	39.9	0.03	0.08	15.8	0.006	0.01
KNRC026	36	37	5,425,582.0	402,781.0	507.1	35.8	0.01	0.09	18	0.018	0.02
KNRC026	37	38	5,425,582.0	402,781.0	506.1	48.4	0.01	0.13	11.3	0.023	0.05
KNRC026	38	39	5,425,582.0	402,781.0	505.1	47.3		0.12	10.3	0.007	
KNRC026	39	40	5,425,582.0	402,781.0	504.1	36.2	0.02	0.1	15.6	0.005	0.02
KNRC026	40	41	5,425,582.0	402,781.0	503.1	30.5	0.03	0.1	19.1	0.008	0.02
KNRC026	41	42	5,425,582.0	402,781.0	502.1	30	0.02	0.08	19.4	0.008	0.02
KNRC026	42	43	5,425,582.0	402,781.0	501.1	24.2		0.06	23.1	0.008	0.03
KNRC026	43	44	5,425,582.0	402,781.0	500.1	25.3		0.07	22.4	0.007	0.02
KNRC026	44	45	5,425,582.0	402,781.0	499.1	38.5	0.02	0.12	15	0.004	0.02
KNRC026	45	46	5,425,582.0	402,781.0	498.1	28.5	0.02	0.08	19.1	0.005	0.02
KNRC026	46	47	5,425,582.0	402,781.0	497.1	21.8	0.03	0.05	22.6	0.005	0.01
KNRC026	50	51	5,425,582.0	402,781.0	493.1	25.9	0.02	0.04	19.8	0.028	
KNRC026	51	52	5,425,582.0	402,781.0	492.1	36.7	0.01	0.07	16.6	0.016	
KNRC026	52	53	5,425,582.0	402,781.0	491.1	35.7	0.04	0.07	17.8	0.038	0.03
KNRC026	53	54	5,425,582.0	402,781.0	490.1	28.4	0.05	0.05	21.4	0.023	0.02
KNRC026	54	55	5,425,582.0	402,781.0	489.1	19		0.03	26.2	0.044	0.02

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC026	55	56	5,425,582.0	402,781.0	488.1	21.5	0.05	0.04	25.3	0.042	0.01
KNRC026	56	57	5,425,582.0	402,781.0	487.1	26	0.06	0.05	21.7	0.023	0.04
KNRC026	57	58	5,425,582.0	402,781.0	486.1	34.1	0.05	0.08	17.5	0.005	0.01
KNRC026	58	59	5,425,582.0	402,781.0	485.1	36.7	0.06	0.08	17.9	0.005	0.01
KNRC026	59	60	5,425,582.0	402,781.0	484.1	35.3	0.06	0.09	18.2	0.004	0.02
KNRC027	5	6	5,425,578.0	402,821.0	537.0	28.2	0.07	0.06	23	0.053	0.05
KNRC027	6	7	5,425,578.0	402,821.0	536.0	32.7	0.1	0.05	22.4	0.06	
KNRC027	7	8	5,425,578.0	402,821.0	535.0	34.8	0.07	0.06	20.8	0.027	0.02
KNRC027	8	9	5,425,578.0	402,821.0	534.0	21.6		0.02	29.8	0.045	0.01
KNRC027	9	10	5,425,578.0	402,821.0	533.0	36.8	0.04	0.05	19.2	0.045	
KNRC027	10	11	5,425,578.0	402,821.0	532.0	46.7	0.02	0.07	13.9	0.053	0.02
KNRC027	11	12	5,425,578.0	402,821.0	531.0	43.9	0.04	0.07	15	0.049	0.02
KNRC027	12	13	5,425,578.0	402,821.0	530.0	34.6		0.05	18.8	0.089	
KNRC027	13	14	5,425,578.0	402,821.0	529.0	25.1	0.06	0.04	23.2	0.032	
KNRC027	14	15	5,425,578.0	402,821.0	528.0	34.1	0.03	0.07	16.3	0.076	0.05
KNRC027	15	16	5,425,578.0	402,821.0	527.0	52.1	0.03	0.09	7.7	0.032	0.03
KNRC027	16	17	5,425,578.0	402,821.0	526.0	34.3	0.03	0.05	17.3	0.064	0.02
KNRC027	17	18	5,425,578.0	402,821.0	525.0	21.8	0.03	0.03	25.2	0.1	0.02
KNRC027	18	19	5,425,578.0	402,821.0	524.0	21.2	0.03	0.02	25.6	0.067	
KNRC027	19	20	5,425,578.0	402,821.0	523.0	27.5	0.02	0.04	21.8	0.095	0.01
KNRC027	20	21	5,425,578.0	402,821.0	522.0	29.5	0.03	0.05	20.8	0.069	0.27
KNRC027	21	22	5,425,578.0	402,821.0	521.0	38.9	0.05	0.07	13.8	0.054	0.25
KNRC027	22	23	5,425,578.0	402,821.0	520.0	40.4	0.01	0.07	14.9	0.067	0.01
KNRC027	23	24	5,425,578.0	402,821.0	519.0	51.8	0.05	0.08	8.4	0.024	0.02
KNRC027	24	25	5,425,578.0	402,821.0	518.0	53.9	0.03	0.09	7.4	0.033	0.02
KNRC027	25	26	5,425,578.0	402,821.0	517.0	51.4	0.03	0.11	9.3	0.024	0.07
KNRC027	26	27	5,425,578.0	402,821.0	516.0	47.3	0.03	0.1	11	0.039	0.01
KNRC027	27	28	5,425,578.0	402,821.0	515.0	49.6	0.03	0.09	10	0.017	0.02
KNRC027	28	29	5,425,578.0	402,821.0	514.0	31.4	0.01	0.04	19.6	0.041	0.02
KNRC027	29	30	5,425,578.0	402,821.0	513.0	30.1		0.05	17.6	0.065	
KNRC027	30	31	5,425,578.0	402,821.0	512.0	17		0.02	28.1	0.038	0.02
KNRC027	31	32	5,425,578.0	402,821.0	511.0	24.7	0.02	0.02	21.2	0.029	0.02
KNRC027	32	33	5,425,578.0	402,821.0	510.0	26.4	0.01	0.03	18.9	0.04	
KNRC030	16	17	5,425,499.0	402,843.0	522.7	28	0.04	0.04	17.9	0.039	0.08
KNRC030	17	18	5,425,499.0	402,843.0	521.7	33.2	0.05	0.05	14.9	0.047	0.02
KNRC030	18	19	5,425,499.0	402,843.0	520.7	29.9	0.15	0.04	21.9	0.023	0.02
KNRC030	19	20	5,425,499.0	402,843.0	519.7	28.3	0.17	0.05	24.4	0.019	0.02
KNRC030	20	21	5,425,499.0	402,843.0	518.7	23	0.16	0.03	28.2	0.013	0.02
KNRC030	21	22	5,425,499.0	402,843.0	517.7	22.6	0.11	0.02	27.6	0.03	0.01
KNRC030	22	23	5,425,499.0	402,843.0	516.7	40.8	0.1	0.1	15.9	0.033	0.01
KNRC030	23	24	5,425,499.0	402,843.0	515.7	31.2	0.14	0.05	22.7	0.042	0.03
KNRC030	24	25	5,425,499.0	402,843.0	514.7	38.4	0.09	0.08	17.4	0.037	0.03
KNRC030	25	26	5,425,499.0	402,843.0	513.7	35.1	0.05	0.07	15.9	0.047	0.02
KNRC030	26	27	5,425,499.0	402,843.0	512.7	21.9	0.04	0.04	20.5	0.029	0.03
KNRC030	27	28	5,425,499.0	402,843.0	511.7	38.7	0.03	0.09	12.2	0.039	0.04
KNRC030	28	29	5,425,499.0	402,843.0	510.7	40.6	0.08	0.11	14.4	0.021	0.21
KNRC030	29	30	5,425,499.0	402,843.0	509.7	38.9	0.04	0.09	13.4	0.059	0.04
KNRC030	30	31	5,425,499.0	402,843.0	508.7	29.9	0.03	0.06	17.8	0.041	0.03
KNRC030	31	32	5,425,499.0	402,843.0	507.7	38.1	0.04	0.08	14.4	0.031	0.05

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC030	32	33	5,425,499.0	402,843.0	506.7	30.2	0.06	0.06	20.3	0.033	0.03
KNRC030	33	34	5,425,499.0	402,843.0	505.7	33.8	0.07	0.05	18.4	0.031	0.07
KNRC030	34	35	5,425,499.0	402,843.0	504.7	29.6	0.03	0.08	15.7	0.037	0.18
KNRC031	27.51	28.51	5,425,502.0	402,799.0	512.2	28.523	0.0796	0.0402	22.509	0.0547	0.04
KNRC031	28.51	29.51	5,425,502.0	402,799.0	511.2	36.486	0.0498	0.0908	17.236	0.0221	0.1114
KNRC031	29.51	30.51	5,425,502.0	402,799.0	510.2	33.611	0.0298	0.0943	16.395	0.0219	0.1035
KNRC031	30.51	31.51	5,425,502.0	402,799.0	509.2	26.749	0.0149	0.0651	18.6	0.018	0.0198
KNRC031	31.51	32.51	5,425,502.0	402,799.0	508.2	31.29	0.01	0.0751	16.407	0.0302	0.01
KNRC031	32.51	33.51	5,425,502.0	402,799.0	507.2	34.527	0.01	0.08	15.575	0.0303	0.0202
KNRC031	33.51	34.51	5,425,502.0	402,799.0	506.2	33.961	0.0151	0.0851	16.137	0.0169	0.0198
KNRC031	34.51	35.51	5,425,502.0	402,799.0	505.2	32.001	0.02	0.0849	16.622	0.0135	0.0916
KNRC031	35.51	36.51	5,425,502.0	402,799.0	504.2	27.611	0.0302	0.0647	20.403	0.0186	0.1241
KNRC031	36.51	37.51	5,425,502.0	402,799.0	503.2	22.079	0.0553	0.0347	25.601	0.0179	0.0545
KNRC031	40.51	41.51	5,425,502.0	402,799.0	499.2	24.357	0.0298	0.0555	22.685	0.0144	0.0302
KNRC031	41.51	42.51	5,425,502.0	402,799.0	498.2	28.58	0.02	0.0698	20.01	0.0191	0.0502
KNRC031	42.51	43.51	5,425,502.0	402,799.0	497.2	33.108	0.02	0.0804	17.44	0.0199	0.0396
KNRC031	43.51	44.51	5,425,502.0	402,799.0	496.2	31.005	0.0353	0.0745	18.478	0.012	0.0149
KNRC031	44.51	45.51	5,425,502.0	402,799.0	495.2	21.299	0.0551	0.0398	24.391	0.0126	0.0151
KNRC031	45.51	46.51	5,425,502.0	402,799.0	494.2	20.687	0.0651	0.03	26.043	0.016	0.02
KNRC031	46.51	47.51	5,425,502.0	402,799.0	493.2	19.185	0.0751	0.0249	27.281	0.015	0.0149
KNRC031	47.51	48.51	5,425,502.0	402,799.0	492.2	23.191	0.0545	0.0506	23.904	0.0156	0.0151
KNRC031	48.51	49.51	5,425,502.0	402,799.0	491.2	31.324	0.0351	0.08	18.588	0.0139	0.02
KNRC031	49.51	50.51	5,425,502.0	402,799.0	490.2	29.848	0.0451	0.0698	19.734	0.0141	0.0149
KNRC031	50.51	51.51	5,425,502.0	402,799.0	489.2	31.176	0.0347	0.0549	17.626	0.0491	0.0202
KNRC031	51.51	52.51	5,425,502.0	402,799.0	488.2	32.452	0.02	0.0449	15.53	0.0668	0.0249
KNRC031	52.51	53.51	5,425,502.0	402,799.0	487.2	30.253	0.02	0.04	17.612	0.0611	0.0251
KNRC031	53.51	54.51	5,425,502.0	402,799.0	486.2	32.593	0.02	0.0451	16.466	0.066	0.0402
KNRC031	54.51	55.51	5,425,502.0	402,799.0	485.2	40.412	0.0302	0.0551	12.709	0.063	0.0398
KNRC031	55.51	56.51	5,425,502.0	402,799.0	484.2	45.288	0.04	0.0702	9.476	0.0513	0.03
KNRC031	56.51	57.51	5,425,502.0	402,799.0	483.2	44.037	0.0655	0.08	8.249	0.0282	0.0453
KNRC031	57.51	58.51	5,425,502.0	402,799.0	482.2	42.788	0.0798	0.0902	10.495	0.017	0.0498
KNRC031	58.51	59.51	5,425,502.0	402,799.0	481.2	36.9615	0.07	0.0902	11.3781	0.019	0.0743
KNRC033	17	18	5,425,420.0	402,840.0	520.0	44.2	0.03	0.12	10.9	0.009	3
KNRC033	18	19	5,425,420.0	402,840.0	519.0	43.4	0.04	0.14	11.9	0.002	0.31
KNRC033	19	20	5,425,420.0	402,840.0	518.0	45.4	0.03	0.14	10.8	0.005	0.04
KNRC033	20	21	5,425,420.0	402,840.0	517.0	15.5	0.02	0.05	23.8	0.016	0.07
KNRC033	21	22	5,425,420.0	402,840.0	516.0	52	0.02	0.17	8.3	0.005	0.17
KNRC033	22	23	5,425,420.0	402,840.0	515.0	51.2		0.14	7	0.005	2
KNRC033	23	24	5,425,420.0	402,840.0	514.0	48.7		0.14	9	0.014	1.4
KNRC033	24	25	5,425,420.0	402,840.0	513.0	41.6	0.06	0.12	13.4	0.003	1.6
KNRC033	25	26	5,425,420.0	402,840.0	512.0	31.5		0.1	18.5	0.012	0.77
KNRC033	26	27	5,425,420.0	402,840.0	511.0	35.6	0.02	0.11	17.3	0.032	0.12
KNRC033	27	28	5,425,420.0	402,840.0	510.0	38.6	0.02	0.13	15	0.015	0.23
KNRC033	28	29	5,425,420.0	402,840.0	509.0	41.2	0.02	0.14	13.9	0.016	0.14
KNRC033	29	30	5,425,420.0	402,840.0	508.0	36.3		0.11	16.4	0.017	0.23
KNRC033	30	31	5,425,420.0	402,840.0	507.0	28.5	0.02	0.09	19	0.024	0.04
KNRC033	31	32	5,425,420.0	402,840.0	506.0	32.8		0.1	17.2	0.05	0.03
KNRC033	32	33	5,425,420.0	402,840.0	505.0	37.2	0.04	0.1	13.4	0.019	0.03
KNRC033	33	34	5,425,420.0	402,840.0	504.0	30.2	0.03	0.09	17.7	0.033	0.03

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC033	34	35	5,425,420.0	402,840.0	503.0	34.2	0.02	0.1	16.2	0.034	0.03
KNRC033	35	36	5,425,420.0	402,840.0	502.0	44.3	0.01	0.11	10.5	0.019	0.03
KNRC033	36	37	5,425,420.0	402,840.0	501.0	41.9	0.03	0.11	13.2	0.021	0.07
KNRC033	37	38	5,425,420.0	402,840.0	500.0	47.8	0.02	0.14	10.3	0.024	0.03
KNRC033	38	39	5,425,420.0	402,840.0	499.0	45.4	0.02	0.12	10.6	0.021	0.13
KNRC033	39	40	5,425,420.0	402,840.0	498.0	40.3	0.04	0.1	13.5	0.02	0.34
KNRC033	40	41	5,425,420.0	402,840.0	497.0	49.7	0.03	0.12	8.7	0.035	0.04
KNRC033	41	42	5,425,420.0	402,840.0	496.0	52.2	0.04	0.13	7.7	0.022	0.03
KNRC033	42	43	5,425,420.0	402,840.0	495.0	38.5	0.02	0.11	13.6	0.051	0.17
KNRC033	43	44	5,425,420.0	402,840.0	494.0	50.3	0.04	0.18	6.1	0.025	0.47
KNRC033	44	45	5,425,420.0	402,840.0	493.0	42.8	0.02	0.16	8.3	0.082	0.41
KNRC033	45	46	5,425,420.0	402,840.0	492.0	44.5	0.03	0.15	8.2	0.055	0.24
KNRC033	46	47	5,425,420.0	402,840.0	491.0	45	0.03	0.13	9.9	0.035	0.54
KNRC033	47	48	5,425,420.0	402,840.0	490.0	47.7	0.04	0.09	6	0.042	0.17
KNRC033	48	49	5,425,420.0	402,840.0	489.0	47.9	0.03	0.07	3.6	0.052	0.14
KNRC033	49	50	5,425,420.0	402,840.0	488.0	47.1	0.04	0.06	4.7	0.046	0.1
KNRC033	50	51	5,425,420.0	402,840.0	487.0	41.1	0.03	0.04	7.7	0.03	0.04
KNRC033	51	52	5,425,420.0	402,840.0	486.0	51.1	0.05	0.04	3.7	0.025	0.04
KNRC033	52	53	5,425,420.0	402,840.0	485.0	35.5		0.05	8.3	0.037	0.05
KNRC033A	40	41	5,425,420.0	402,804.0	497.0	26.6	0.1	0.05	22.5	0.068	0.07
KNRC033A	41	42	5,425,420.0	402,804.0	496.0	30.4	0.08	0.09	18.3	0.076	3.1
KNRC033A	42	43	5,425,420.0	402,804.0	495.0	28.2	0.09	0.06	23.5	0.046	0.77
KNRC033A	43	44	5,425,420.0	402,804.0	494.0	47.8	0.05	0.11	12	0.024	0.7
KNRC033A	44	45	5,425,420.0	402,804.0	493.0	28.8	0.06	0.06	24.2	0.044	0.2
KNRC033A	45	46	5,425,420.0	402,804.0	492.0	30.3	0.06	0.06	23.5	0.023	0.45
KNRC033A	46	47	5,425,420.0	402,804.0	491.0	42.5	0.07	0.1	13.9	0.05	0.87
KNRC033A	47	48	5,425,420.0	402,804.0	490.0	35.4	0.03	0.05	18.7	0.023	0.18
KNRC033A	48	49	5,425,420.0	402,804.0	489.0	47.7	0.03	0.08	11.5	0.017	0.47
KNRC033A	49	50	5,425,420.0	402,804.0	488.0	46.9	0.02	0.09	12.5	0.051	0.11
KNRC033A	50	51	5,425,420.0	402,804.0	487.0	34	0.03	0.07	18.6	0.042	0.03
KNRC033A	51	52	5,425,420.0	402,804.0	486.0	37	0.04	0.09	17.5	0.024	0.31
KNRC033A	52	53	5,425,420.0	402,804.0	485.0	19	0.04	0.04	24.9	0.027	0.04
KNRC033A	54	55	5,425,420.0	402,804.0	483.0	21.1	0.05	0.07	24.8	0.05	0.34
KNRC033A	55	56	5,425,420.0	402,804.0	482.0	22.9	0.02	0.05	19.9	0.068	0.04
KNRC033A	56	57	5,425,420.0	402,804.0	481.0	21.8	0.03	0.06	20.7	0.053	0.04
KNRC033A	57	58	5,425,420.0	402,804.0	480.0	14.5	0.04	0.04	27.8	0.054	0.3
KNRC033A	60	61	5,425,420.0	402,804.0	477.0	9.2	0.02	0.03	10.3	0.014	0.56
KNRC033A	61	62	5,425,420.0	402,804.0	476.0	31.9	0.04	0.09	10.5	0.025	0.11
KNRC033A	62	63	5,425,420.0	402,804.0	475.0	44.5	0.04	0.17	7.6	0.012	0.27
KNRC033A	63	64	5,425,420.0	402,804.0	474.0	24.7	0.03	0.1	12	0.01	0.19
KNRC033A	64	65	5,425,420.0	402,804.0	473.0	10.9	0.03	0.02	16.7	0.024	0.1
KNRC033A	66	67	5,425,420.0	402,804.0	471.0	17.8	0.02	0.02	26.2	0.045	0.09
KNRC033A	67	68	5,425,420.0	402,804.0	470.0	30.4		0.02	14.6	0.065	0.02
KNRC033A	68	69	5,425,420.0	402,804.0	469.0	39.8		0.02	9.5	0.086	0.02
KNRC033A	69	70	5,425,420.0	402,804.0	468.0	30.5	0.02	0.04	16.1	0.056	0.17
KNRC033A	70	71	5,425,420.0	402,804.0	467.0	34.6	0.07	0.06	16.5	0.12	0.03
KNRC033A	71	72	5,425,420.0	402,804.0	466.0	42.1	0.02	0.09	12.8	0.098	0.05
KNRC033A	72	73	5,425,420.0	402,804.0	465.0	35.7	0.01	0.04	16.4	0.088	0.09
KNRC033A	73	74	5,425,420.0	402,804.0	464.0	36.8	0.05	0.04	18.3	0.078	0.02

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC035	8	9	5,425,407.0	402,902.0	530.5	51.9	0.06	0.06	1.3	0.075	0.11
KNRC035	9	10	5,425,407.0	402,902.0	529.5	63.1	0.05	0.09	0.2	0.064	0.03
KNRC035	10	11	5,425,407.0	402,902.0	528.5	62.5	0.05	0.1	0.47	0.059	0.02
KNRC035	11	12	5,425,407.0	402,902.0	527.5	64.1	0.06	0.11	0.56	0.033	
KNRC035	12	13	5,425,407.0	402,902.0	526.5	60.9	0.06	0.08	0.87	0.026	
KNRC035	13	14	5,425,407.0	402,902.0	525.5	53.7	0.04	0.08	3.1	0.023	0.02
KNRC035	14	15	5,425,407.0	402,902.0	524.5	45	0.06	0.08	0.66	0.044	0.04
KNRC035	17	18	5,425,407.0	402,902.0	521.5	43.6	0.05	0.07	5.2	0.058	0.04
KNRC035	18	19	5,425,407.0	402,902.0	520.5	46.5	0.05	0.08	4.1	0.039	0.03
KNRC035	19	20	5,425,407.0	402,902.0	519.5	59.9	0.03	0.08	0.5	0.017	
KNRC035	20	21	5,425,407.0	402,902.0	518.5	44.1	0.02	0.08	5.3	0.036	0.01
KNRC035	22	23	5,425,407.0	402,902.0	516.5	49.6	0.05	0.08	2.6	0.025	
KNRC035	23	24	5,425,407.0	402,902.0	515.5	49.1	0.02	0.05	1.5	0.027	
KNRC035	24	25	5,425,407.0	402,902.0	514.5	43.7	0.02	0.05	3	0.029	
KNRC035	25	26	5,425,407.0	402,902.0	513.5	40.9	0.01	0.05	3.4	0.044	
KNRC035	26	27	5,425,407.0	402,902.0	512.5	47.5	0.02	0.05	2.6	0.044	
KNRC035	27	28	5,425,407.0	402,902.0	511.5	54.5	0.04	0.08	4.1	0.023	
KNRC035	28	29	5,425,407.0	402,902.0	510.5	56.3	0.05	0.09	4.6	0.005	
KNRC036	30.69	31.69	5,425,502.0	402,559.0	511.2	30.08	0.1731	0.0569	17.003	0.0262	0.06
KNRC036	31.69	32.69	5,425,502.0	402,559.0	510.2	31.666	0.1562	0.0669	14.461	0.1677	0.0669
KNRC036	32.69	33.69	5,425,502.0	402,559.0	509.2	30.444	0.15	0.0631	12.258	0.1148	0.0769
KNRC036	33.69	34.69	5,425,502.0	402,559.0	508.2	32.736	0.3156	0.0669	9.837	0.0844	0.0524
KNRC036	34.69	35.69	5,425,502.0	402,559.0	507.2	33.686	0.2658	0.0631	8.517	0.0919	0.0538
KNRC036	35.69	36.69	5,425,502.0	402,559.0	506.2	36.812	0.21	0.06	6.161	0.0972	0.0393
KNRC036	36.69	37.69	5,425,502.0	402,559.0	505.2	43.268	0.2031	0.0669	3.82	0.0634	0.03
KNRC036	37.69	38.69	5,425,502.0	402,559.0	504.2	50.192	0.2828	0.0631	2.096	0.058	0.02
KNRC036	38.69	39.69	5,425,502.0	402,559.0	503.2	44.986	0.2855	0.1014	4.36	0.0533	0.0614
KNRC036	39.69	40.69	5,425,502.0	402,559.0	502.2	42.39	0.27	0.0924	5.669	0.0235	0.0386
KNRC036	40.69	41.69	5,425,502.0	402,559.0	501.2	44.977	0.2424	0.08	3.975	0.0148	0.02
KNRC036	41.69	42.69	5,425,502.0	402,559.0	500.2	46.483	0.2438	0.08	3.614	0.0229	0.0269
KNRC036	42.69	43.69	5,425,502.0	402,559.0	499.2	44.354	0.2086	0.0731	5.939	0.017	0.0783
KNRC037	14	15	5,425,496.0	402,598.0	528.2	35.9	0.14	0.07	19.6	0.024	0.01
KNRC037	15	16	5,425,496.0	402,598.0	527.2	52.8	0.07	0.13	8.6	0.028	0.02
KNRC037	16	17	5,425,496.0	402,598.0	526.2	49.8	0.07	0.12	9.3	0.028	0.03
KNRC037	17	18	5,425,496.0	402,598.0	525.2	56.3	0.06	0.15	7.3	0.05	
KNRC037	18	19	5,425,496.0	402,598.0	524.2	53	0.07	0.13	9	0.026	0.01
KNRC037	19	20	5,425,496.0	402,598.0	523.2	45.4	0.09	0.1	12.9	0.026	0.02
KNRC037	20	21	5,425,496.0	402,598.0	522.2	46.8	0.09	0.11	12.4	0.019	0.02
KNRC037	21	22	5,425,496.0	402,598.0	521.2	50.9	0.08	0.11	9.4	0.028	
KNRC037	22	23	5,425,496.0	402,598.0	520.2	51.2	0.07	0.11	9.6	0.03	
KNRC037	23	24	5,425,496.0	402,598.0	519.2	51	0.09	0.12	10.4	0.02	
KNRC037	24	25	5,425,496.0	402,598.0	518.2	45.7	0.1	0.1	12.8	0.028	
KNRC037	25	26	5,425,496.0	402,598.0	517.2	48.5	0.08	0.12	10.9	0.023	
KNRC037	26	27	5,425,496.0	402,598.0	516.2	30.4	0.16	0.05	23.4	0.022	
KNRC037	46.99	47.99	5,425,496.0	402,598.0	495.2	27.6	0.15	0.03	24.9		
KNRC037	47.99	48.99	5,425,496.0	402,598.0	494.2	34.629	0.1302	0.0597	20.94	0.002	
KNRC037	48.99	49.99	5,425,496.0	402,598.0	493.2	32.621	0.0904	0.06	21.593	0.005	0.01
KNRC037	49.99	50.99	5,425,496.0	402,598.0	492.2	36.956	0.1197	0.0699	19.323	0.006	0.01
KNRC037	50.99	51.99	5,425,496.0	402,598.0	491.2	40.366	0.0903	0.0601	16.231	0.0149	0.01

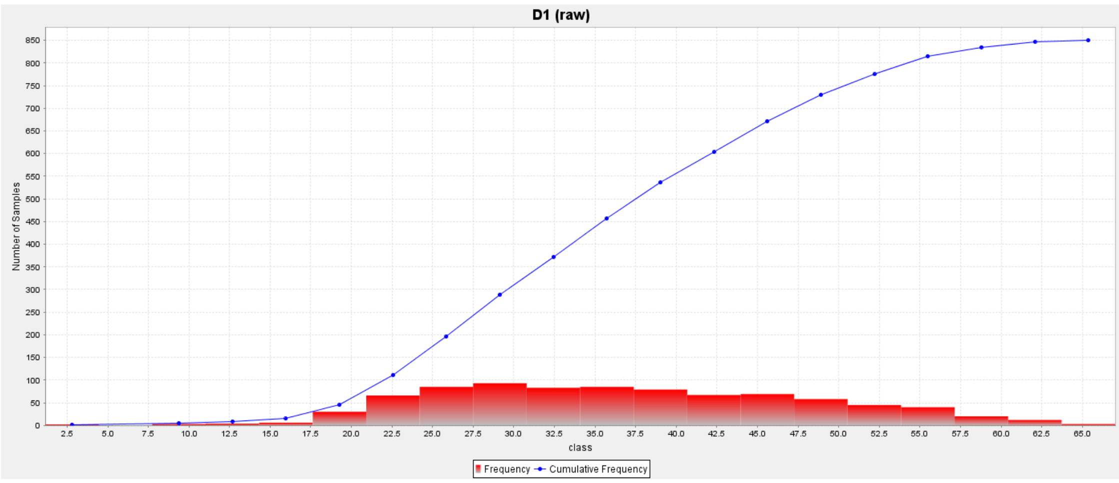
BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC037	51.99	52.99	5,425,496.0	402,598.0	490.2	55.646	0.0801	0.1293	7.686	0.017	0.0199
KNRC037	52.99	53.99	5,425,496.0	402,598.0	489.2	37.782	0.1097	0.0706	18.688	0.0111	0.0101
KNRC037	53.99	54.99	5,425,496.0	402,598.0	488.2	35.422	0.11	0.0601	20.186	0.008	0.01
KNRC037	54.99	55.99	5,425,496.0	402,598.0	487.2	39.36	0.0902	0.0798	17.626	0.011	0.01
KNRC037	55.99	56.99	5,425,496.0	402,598.0	486.2	41.182	0.09	0.0602	16.016	0.0209	0.0199
KNRC037	56.99	57.99	5,425,496.0	402,598.0	485.2	34.666	0.0999	0.0501	20.95	0.0596	0.0101
KNRC037	57.99	58.99	5,425,496.0	402,598.0	484.2	35.194	0.1	0.0599	20.802	0.0224	0.0496
KNRC037	58.99	59.99	5,425,496.0	402,598.0	483.2	36.883	0.1099	0.0699	19.711	0.0161	0.05
KNRC037	59.99	60.99	5,425,496.0	402,598.0	482.2	29.871	0.1298	0.0403	23.957	0.016	0.01
KNRC037	60.99	61.99	5,425,496.0	402,598.0	481.2	24.751	0.1498	0.0301	27.069	0.0219	0.0199
KNRC037	61.99	62.99	5,425,496.0	402,598.0	480.2	18.562	0.1698	0.0102	30.763	0.0131	0.0101
KNRC037	65.99	66.99	5,425,496.0	402,598.0	476.2	20.8	0.14	0.02	26.1	0.007	0.03
KNRC037	66.99	67.99	5,425,496.0	402,598.0	475.2	52.975	0.0509	0.1487	8.082	0.007	0.03
KNRC037	67.99	68.99	5,425,496.0	402,598.0	474.2	50.132	0.0599	0.1401	9.385	0.002	0.01
KNRC037	68.99	69.99	5,425,496.0	402,598.0	473.2	53.169	0.06	0.1598	8.707	0.0109	0.0298
KNRC037	69.99	70.99	5,425,496.0	402,598.0	472.2	51.814	0.0699	0.1402	9.393	0.0189	0.03
KNRC037	70.99	71.99	5,425,496.0	402,598.0	471.2	52.691	0.0898	0.1598	9.598	0.0269	
KNRC037	71.99	72.99	5,425,496.0	402,598.0	470.2	50.621	0.0999	0.1105	10.392	0.031	
KNRC037	72.99	73.99	5,425,496.0	402,598.0	469.2	50.105	0.1099	0.1001	8.915	0.0577	0.01
KNRC037	73.99	74.99	5,425,496.0	402,598.0	468.2	39.111	0.11	0.0505	14.741	0.0996	0.01
KNRC037	74.99	75.99	5,425,496.0	402,598.0	467.2	39	0.1298	0.05	14.899	0.0515	0.01
KNRC037	75.99	76.99	5,425,496.0	402,598.0	466.2	46.821	0.0805	0.0896	9.95	0.1193	0.01
KNRC037	76.99	77.99	5,425,496.0	402,598.0	465.2	50.86	0.08	0.1197	9.108	0.0992	0.01
KNRC037	77.99	78.99	5,425,496.0	402,598.0	464.2	53.078	0.1295	0.12	6.823	0.0277	0.02
KNRC037	78.99	79.99	5,425,496.0	402,598.0	463.2	56.367	0.0607	0.1299	5.81	0.0121	0.0101
KNRC037	79.99	80.99	5,425,496.0	402,598.0	462.2	44.619	0.1095	0.1003	14.809	0.0229	0.0199
KNRC037	80.99	81.99	5,425,496.0	402,598.0	461.2	33.313	0.11	0.0604	22.424	0.021	0.0101
KNRC037	81.99	82.99	5,425,496.0	402,598.0	460.2	25.676	0.1001	0.0501	27.549	0.0121	0.0298
KNRC037	82.99	83.99	5,425,496.0	402,598.0	459.2	36.094	0.1099	0.0698	20.373	0.0259	0.03
KNRC037	83.99	84.99	5,425,496.0	402,598.0	458.2	38.378	0.0803	0.0799	18.617	0.0161	0.04
KNRC037	84.99	85.99	5,425,496.0	402,598.0	457.2	67.011	0.0107	0.1889	1.572	0.016	0.0301
KNRC037	85.99	86.99	5,425,496.0	402,598.0	456.2	61.657	0.0496	0.1702	3.974	0.013	0.0201
KNRC037	86.99	87.99	5,425,496.0	402,598.0	455.2	40.909	0.1391	0.0908	17.563	0.0962	0.0101
KNRC037	87.99	88.99	5,425,496.0	402,598.0	454.2	52.976	0.0905	0.1395	10.077	0.0198	0.0199
KNRC037	88.99	89.99	5,425,496.0	402,598.0	453.2	53.001	0.0702	0.1499	9.901	0.015	0.0794
KNRC037	89.99	90.99	5,425,496.0	402,598.0	452.2	43.298	0.0997	0.1104	15.345	0.0308	0.0107
KNRC037	90.99	91.99	5,425,496.0	402,598.0	451.2	44.883	0.1099	0.0902	15.004	0.0231	0.01
KNRC037	91.99	92.99	5,425,496.0	402,598.0	450.2	40.148	0.1001	0.0999	15.198	0.0299	0.1585
KNRC037	92.99	93.99	5,425,496.0	402,598.0	449.2	41.189	0.1	0.1	16.685	0.032	0.0313
KNRC037	93.99	94.99	5,425,496.0	402,598.0	448.2	41.596	0.0901	0.1	16.205	0.0171	0.0201
KNRC037	94.99	95.99	5,425,496.0	402,598.0	447.2	40.412	0.1197	0.0802	18.081	0.0101	0.02
KNRC037	95.99	96.99	5,425,496.0	402,598.0	446.2	37.826	0.12	0.0701	19.882	0.012	0.0299
KNRC037	96.99	97.99	5,425,496.0	402,598.0	445.2	42.849	0.0804	0.0898	16.732	0.0189	0.03
KNRC037	97.99	98.99	5,425,496.0	402,598.0	444.2	38.346	0.0998	0.0801	19.175	0.0358	
KNRC037	98.99	99.99	5,425,496.0	402,598.0	443.2	37.706	0.1297	0.0701	19.695	0.0162	
KNRC037	97.56	98.56	5,425,496.0	402,598.0	444.7	40.324	0.0912	0.0844	18.1	0.0285	
KNRC037	98.56	99.56	5,425,496.0	402,598.0	443.7	37.964	0.1168	0.0744	19.48	0.0248	
KNRC043	28	29	5,425,436.0	402,507.0	514.5	26.6	0.09	0.14	21.3	0.024	0.02
KNRC043	29	30	5,425,436.0	402,507.0	513.5	29	0.11	0.1	19.9	0.023	0.07

BHID	From	To	y	x	z	Fe %	SnO2 %	WO3 %	CaO %	P2O5 %	SO3 %
KNRC043	30	31	5,425,436.0	402,507.0	512.5	30.7	0.11	0.09	19.4	0.027	0.05
KNRC043	31	32	5,425,436.0	402,507.0	511.5	31.3	0.17	0.09	19.3	0.026	0.08
KNRC043	32	33	5,425,436.0	402,507.0	510.5	29.7	0.11	0.11	18.8	0.033	0.02
KNRC043	33	34	5,425,436.0	402,507.0	509.5	29.3	0.11	0.07	20.9	0.024	0.03
KNRC043	34	35	5,425,436.0	402,507.0	508.5	30.3	0.13	0.09	17.2	0.028	0.17
KNRC043	35	36	5,425,436.0	402,507.0	507.5	32.8	0.08	0.13	14.9	0.022	0.07
KNRC043	36	37	5,425,436.0	402,507.0	506.5	32.4	0.07	0.12	14.6	0.024	0.04
KNRC043	37	38	5,425,436.0	402,507.0	505.5	36.1	0.11	0.09	15.1	0.023	0.05
KNRC043	38	39	5,425,436.0	402,507.0	504.5	31.6	0.16	0.07	19.9	0.025	0.05
KNRC043	39	40	5,425,436.0	402,507.0	503.5	25	0.26	0.05	23.4	0.037	0.29
KNRC043	40	41	5,425,436.0	402,507.0	502.5	43.2	0.54	0.06	10	0.018	0.21
KNRC043	41	42	5,425,436.0	402,507.0	501.5	42.3	0.53	0.05	10.4	0.015	0.07
KNRC043	42	43	5,425,436.0	402,507.0	500.5	26.3	0.27	0.04	20.7	0.007	0.1
KNRC043	43	44	5,425,436.0	402,507.0	499.5	15.7	0.09	0.02	12.2	0.021	0.13
KNRC043	44	45	5,425,436.0	402,507.0	498.5	22	0.19	0.02	18.7	0.004	0.04
KNRC043	45	46	5,425,436.0	402,507.0	497.5	25.8	0.18	0.06	20.2	0.01	0.47
KNRC043	46	47	5,425,436.0	402,507.0	496.5	23.8	0.17	0.06	22.4	0.025	0.28
KNRC043	47	48	5,425,436.0	402,507.0	495.5	34	0.22	0.06	13.3	0.033	0.54
KNRC043	48	49	5,425,436.0	402,507.0	494.5	25.1	0.22	0.02	24.7	0.035	0.02
KNRC043	49	50	5,425,436.0	402,507.0	493.5	26.9	0.2	0.04	17.7	0.02	0.03
KNRC043	50	51	5,425,436.0	402,507.0	492.5	30.2	0.26	0.04	14.7	0.023	0.03
KNRC043	51	52	5,425,436.0	402,507.0	491.5	22.5	0.32	0.03	21	0.028	0.05
KNRC043	56	57	5,425,436.0	402,507.0	486.5	17.5	0.18	0.14	22.5	0.008	0.14
KNRC043	57	58	5,425,436.0	402,507.0	485.5	24	0.26	0.04	20.3	0.019	0.05
KNRC043	58	59	5,425,436.0	402,507.0	484.5	31.1	0.25	0.17	11.8	0.025	0.2
KNRC043	59	60	5,425,436.0	402,507.0	483.5	32.9	0.3	0.05	9.9	0.028	0.07
KNRC043	60	61	5,425,436.0	402,507.0	482.5	21.4	0.14	0.04	19.8	0.027	0.04
KNRC043	61	62	5,425,436.0	402,507.0	481.5	34.5	0.12	0.04	14.9	0.023	0.02
KNRC043	62	63	5,425,436.0	402,507.0	480.5	27.6	0.17	0.03	23.2	0.025	0.02
KNRC043	63	64	5,425,436.0	402,507.0	479.5	26.5	0.17	0.02	23.3	0.029	0.01
KNRC043	64	65	5,425,436.0	402,507.0	478.5	27.5	0.1	0.04	21.1	0.046	0.03
KNRC043	65	66	5,425,436.0	402,507.0	477.5	31.4	0.03	0.05	18.4	0.025	0.04
KNRC044	3	4	5,426,029.0	402,785.0	532.9	37.9	0.48	0.04	4.7	0.05	0.06
KNRC044	4	5	5,426,029.0	402,785.0	531.9	30.8	0.41	0.03	13.5	0.049	0.05
KNRC044	5	6	5,426,029.0	402,785.0	530.9	25.8	0.2	0.04	20.5	0.019	0.02
KNRC044	6	7	5,426,029.0	402,785.0	529.9	30	0.26	0.05	15.7	0.025	0.03
KNRC044	7	8	5,426,029.0	402,785.0	528.9	33.3	0.17	0.07	15.1	0.017	0.03
KNRC044	8	9	5,426,029.0	402,785.0	527.9	34.7	0.19	0.06	13.8	0.021	0.02
KNRC044	9	10	5,426,029.0	402,785.0	526.9	35.2	0.14	0.07	14.4	0.016	0.02
KNRC044	10	11	5,426,029.0	402,785.0	525.9	41.4	0.1	0.09	16	0.009	
KNRC044	11	12	5,426,029.0	402,785.0	524.9	38	0.12	0.07	18.4	0.008	0.01
KNRC044	12	13	5,426,029.0	402,785.0	523.9	31.3	0.12	0.04	23.7	0.008	
KNRC045	0	1	5,426,017.0	402,839.0	535.5	50.3	0.09	0.07	0.79	0.046	0.05
KNRC045	1	2	5,426,017.0	402,839.0	534.5	56.5	0.06	0.13	3.6	0.055	0.02
KNRC045	2	3	5,426,017.0	402,839.0	533.5	52	0.06	0.07	5.3	0.054	0.01
KNRC045	3	4	5,426,017.0	402,839.0	532.5	41.5	0.1	0.06	11.7	0.047	0.02
KNRC045	4	5	5,426,017.0	402,839.0	531.5	34.7	0.14	0.05	19.8	0.035	
KNRC045	5	6	5,426,017.0	402,839.0	530.5	50.9	0.06	0.12	8.6	0.029	
KNRC045	6	7	5,426,017.0	402,839.0	529.5	45.1	0.03	0.09	11.1	0.11	

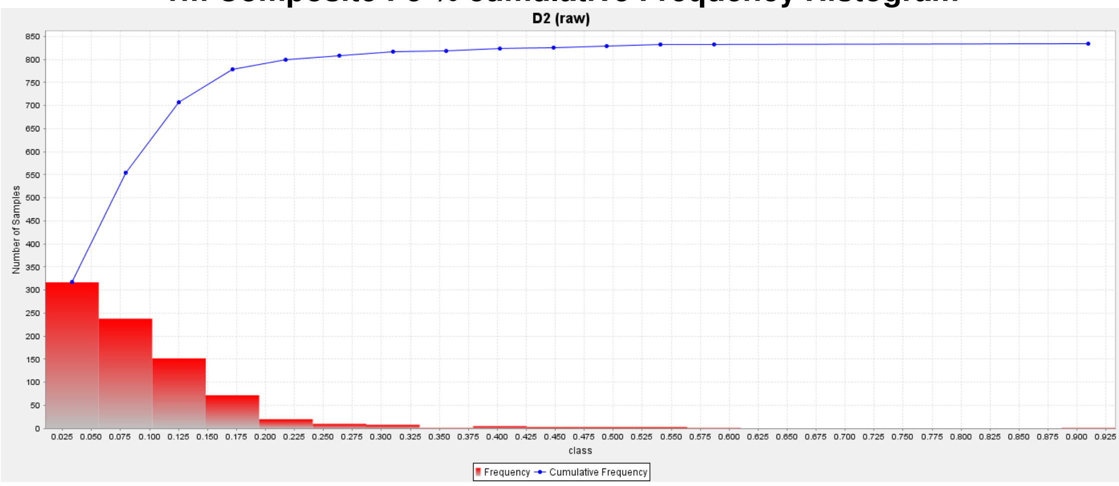
Appendix 2.

1m composite Basic Statistics

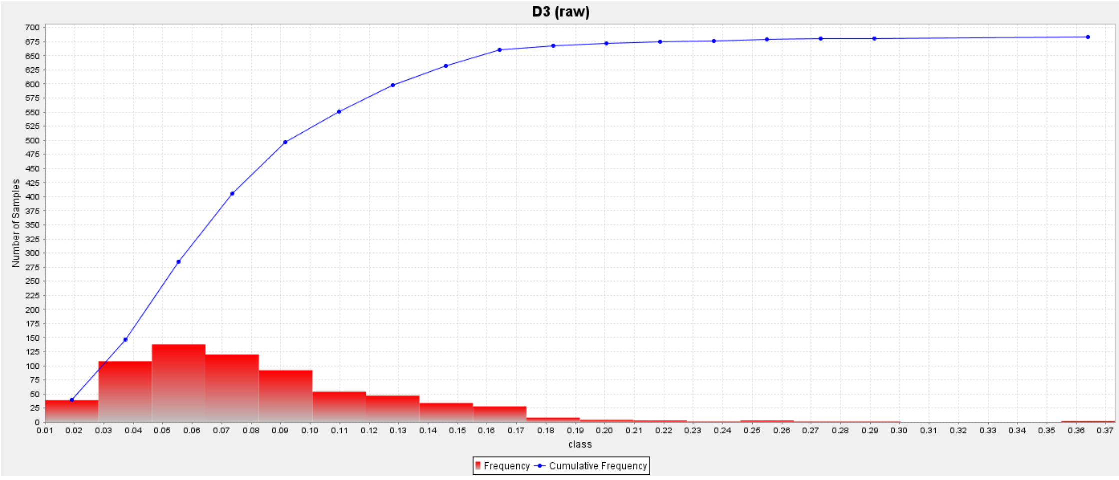
Variable	Fe %	SnO2 %	WO3 %	CaO %	P2O5%	SO3 %
Number of samples	861	838	685	687	684	521
Minimum value	1.15	0.01	0.01	0.15	0.002	0.01
Maximum value	67.01	0.76	0.41	43.00	0.25	19.60
Mean	37.01	0.09	0.08	14.81	0.04	0.36
Median	35.90	0.08	0.07	15.00	0.03	0.03
Geometric Mean	34.99	0.07	0.07	12.21	0.03	0.06
Variance	131.53	0.007	0.002	49.74	0.001	2.22
Standard Deviation	11.47	0.08	0.05	7.05	0.03	1.49
Coefficient of variation	0.31	0.89	0.57	0.48	0.83	4.12
Skewness	0.16	3.14	1.59	-0.01	2.21	8.47
Kurtosis	2.44	18.80	8.34	2.58	9.98	87.83
Natural Log Mean	3.56	-2.67	-2.65	2.50	-3.53	-2.88
Log Variance	0.13	0.65	0.35	0.60	0.63	2.39



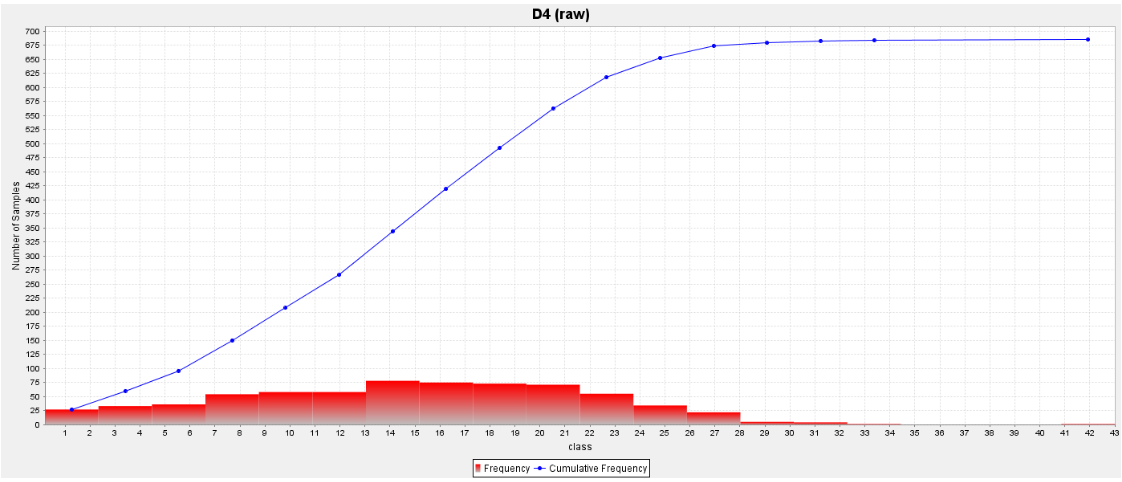
1m Composite Fe % cumulative Frequency Histogram



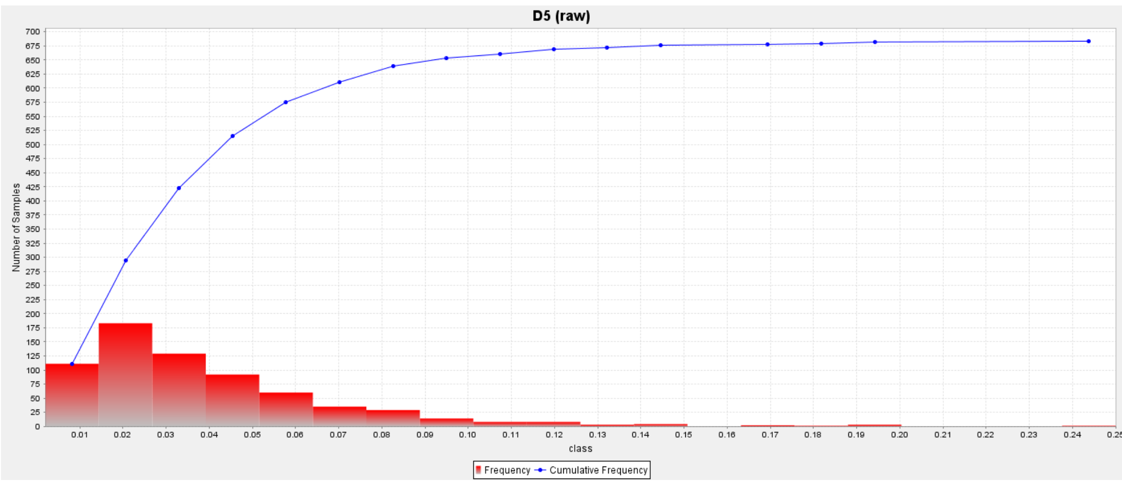
1m Composite SnO_2 % cumulative Frequency Histogram



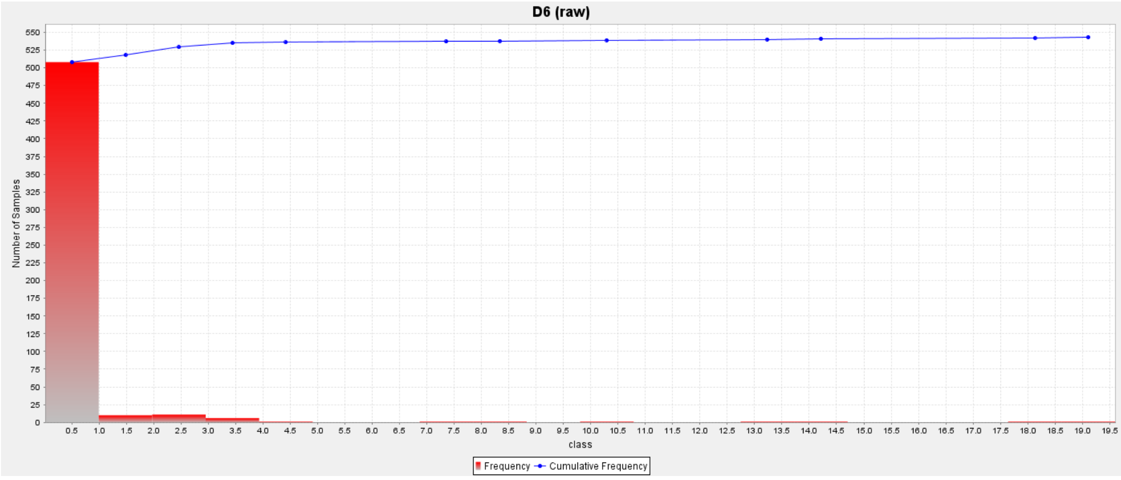
1m Composite WO_3 % cumulative Frequency Histogram



1m Composite CaO % cumulative Frequency Histogram



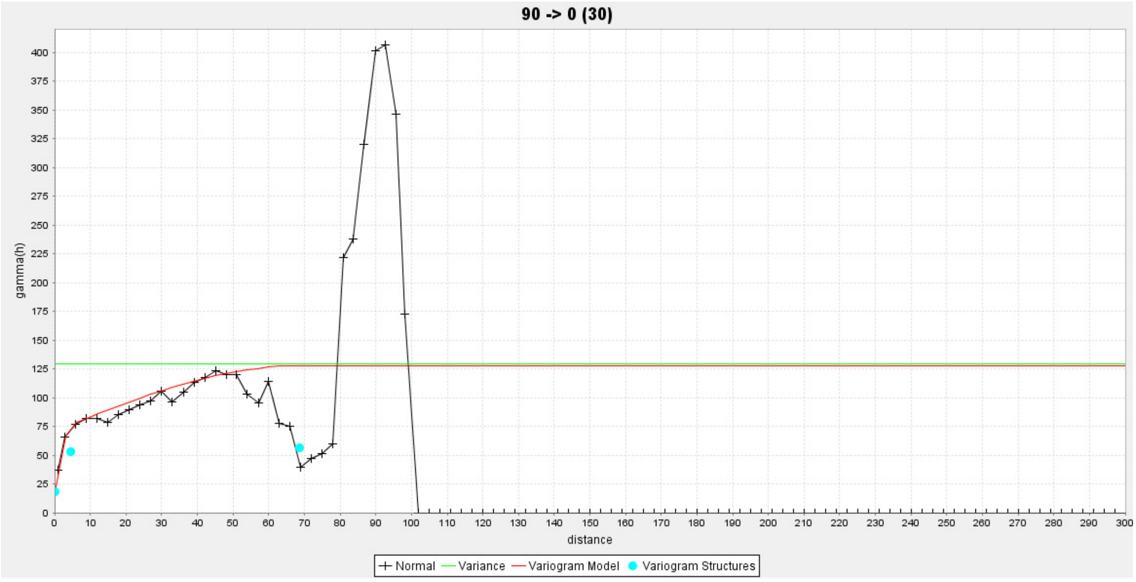
1m Composite P_2O_5 % cumulative Frequency Histogram



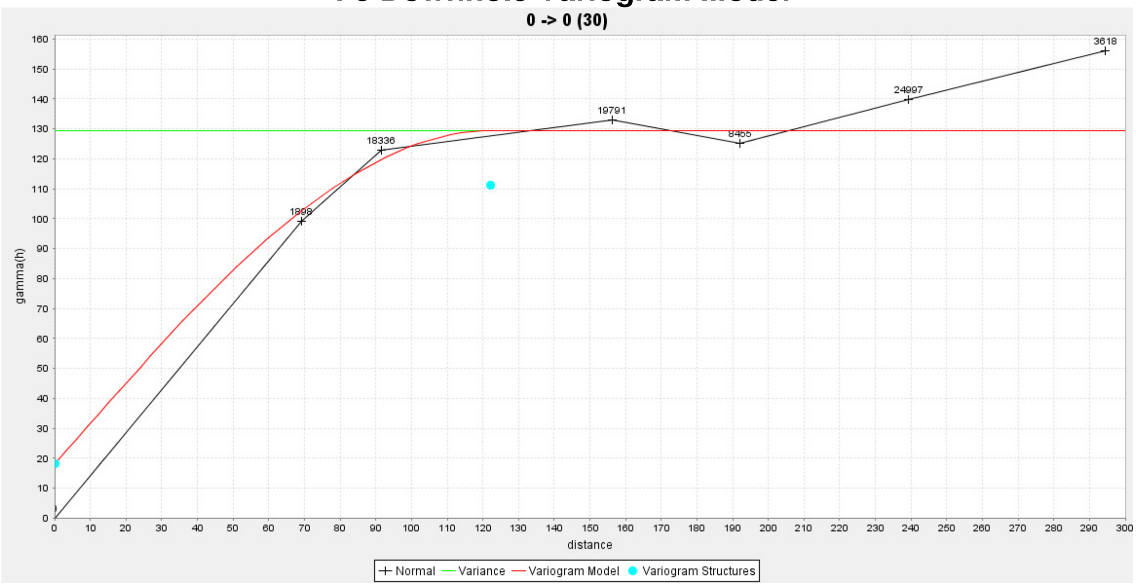
1m Composite SO_3 % cumulative Frequency Histogram

Appendix 3

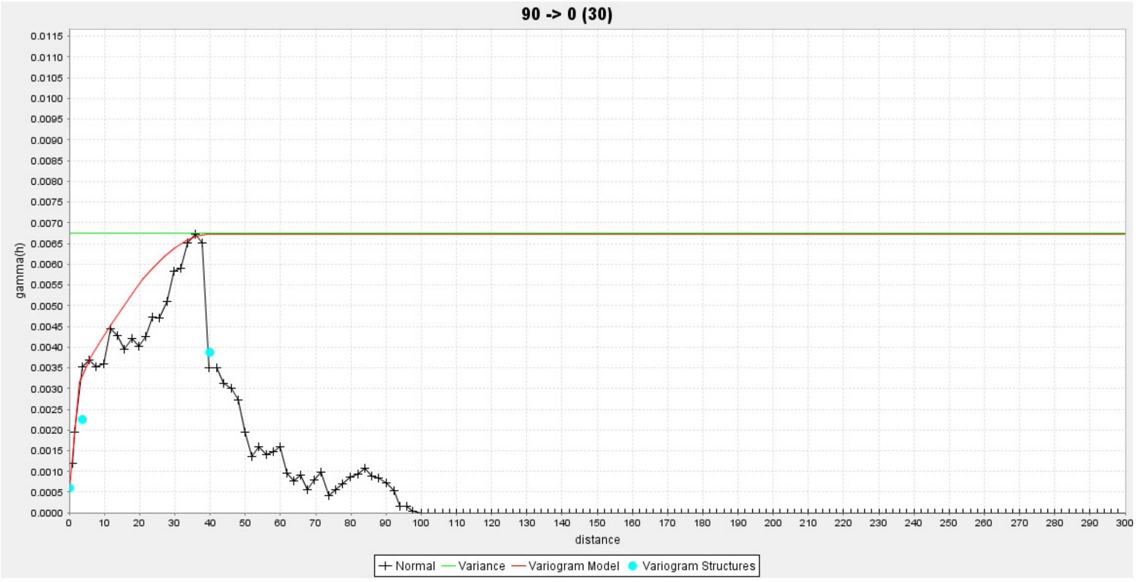
Kara No 2 North Semi Variogram Models



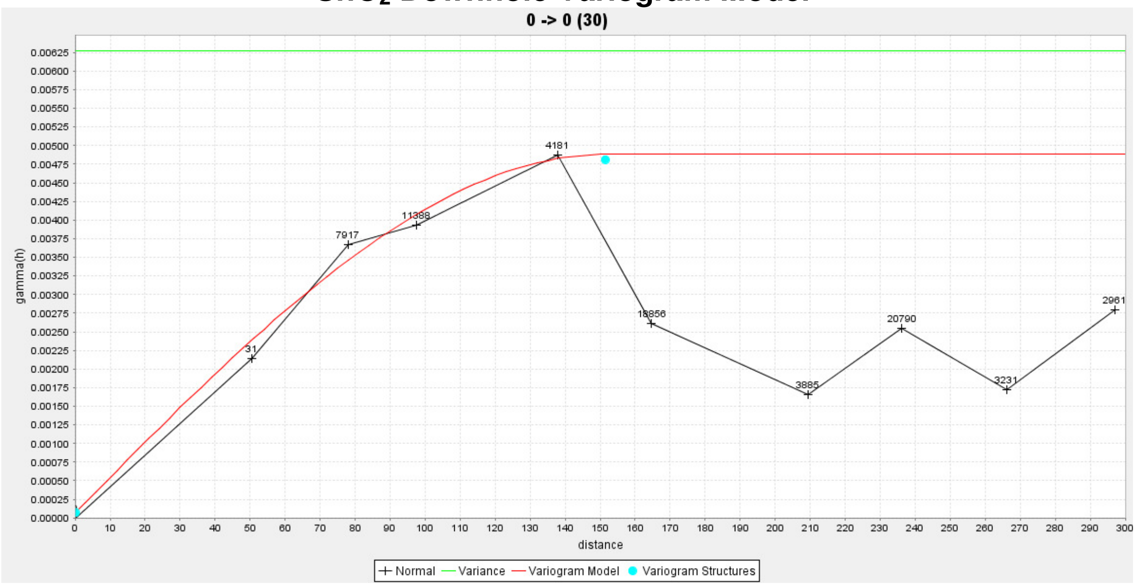
Fe Downhole Variogram Model



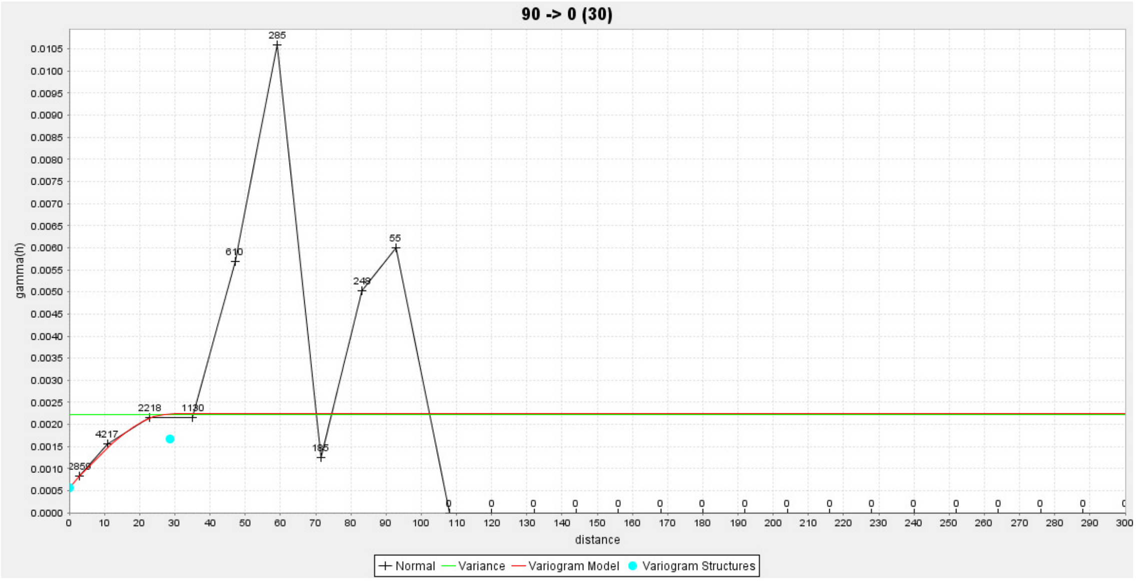
Fe Horizontal Variogram Model



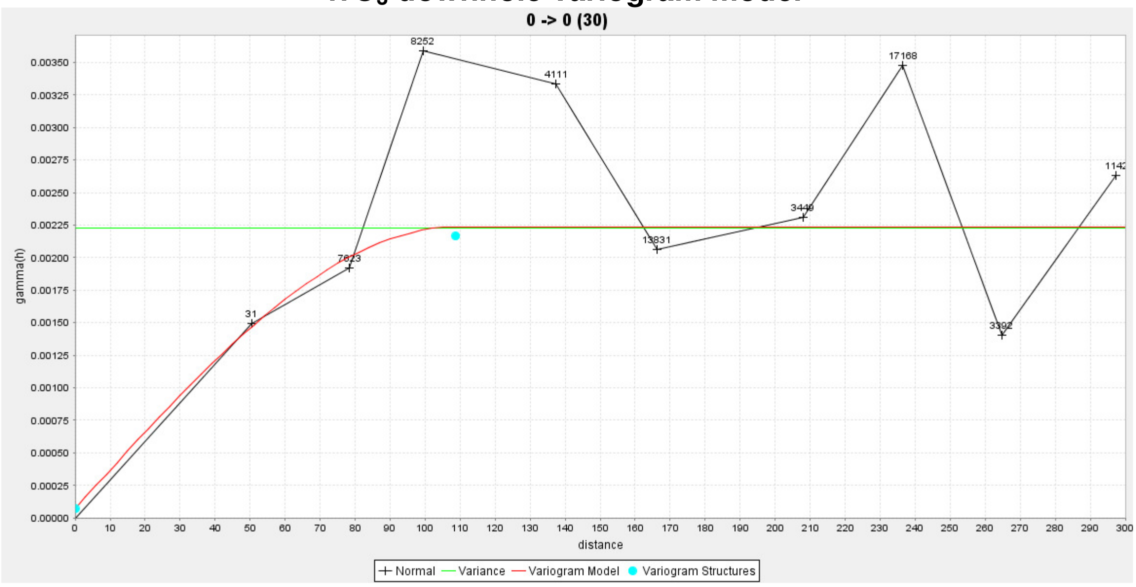
SnO_2 Downhole Variogram Model



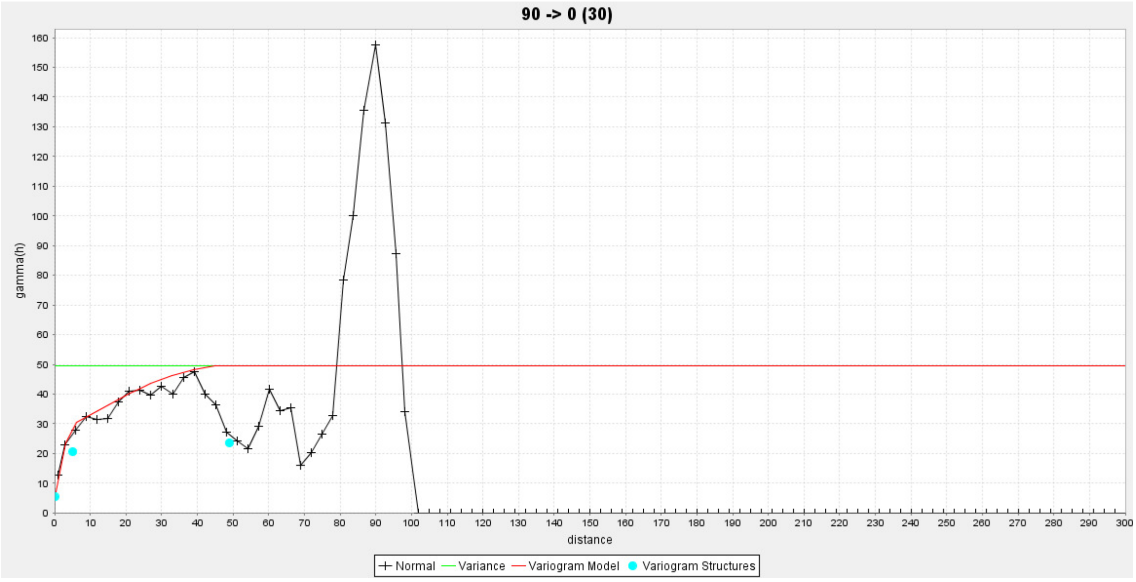
SnO_2 Horizontal Variogram



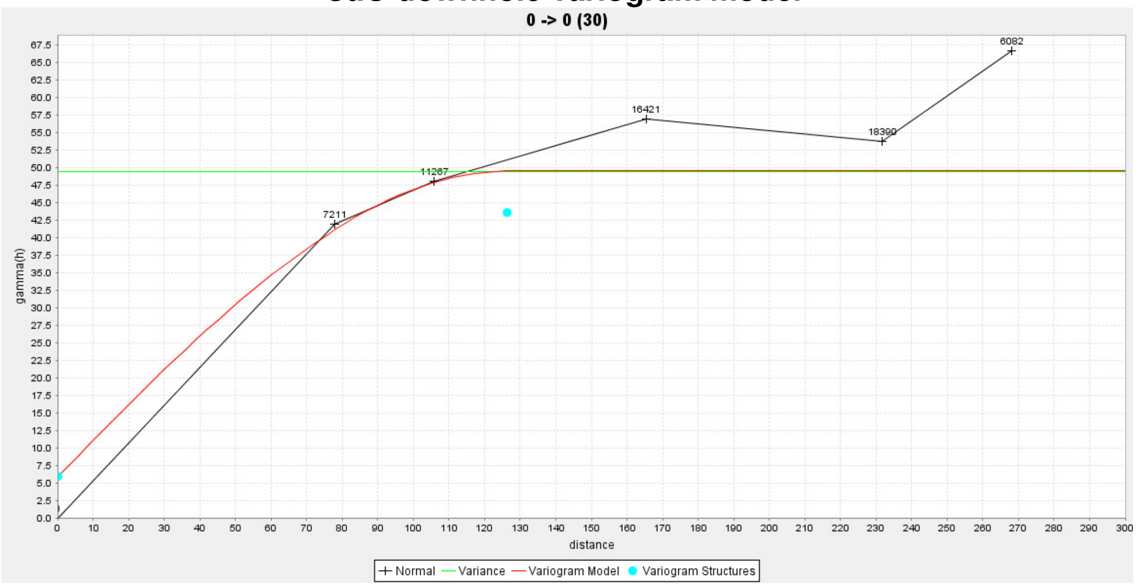
WO_3 downhole variogram model



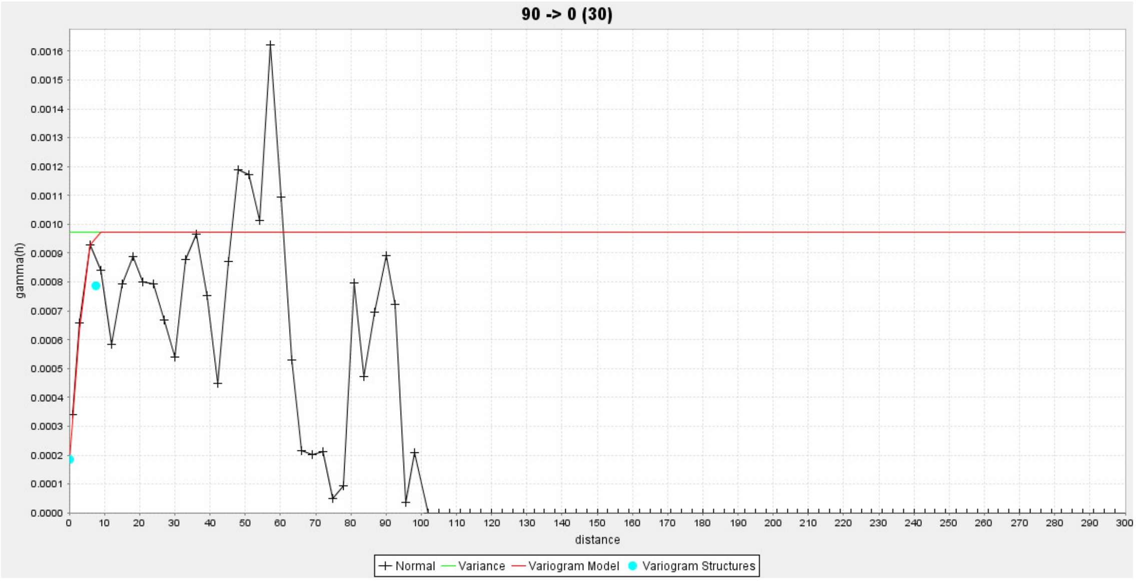
WO_3 horizontal variogram model



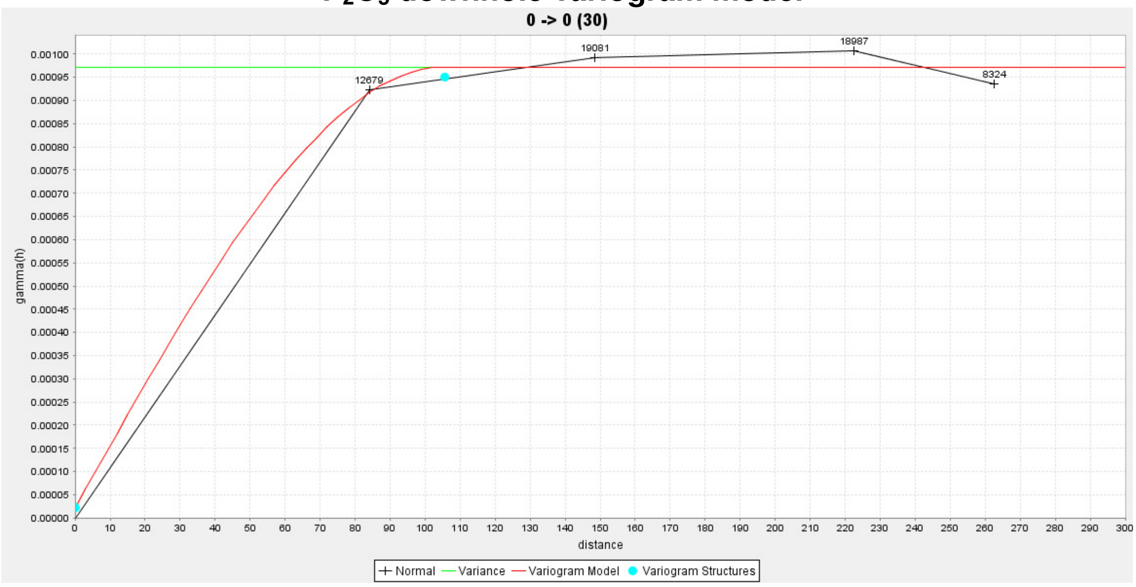
CaO downhole variogram model



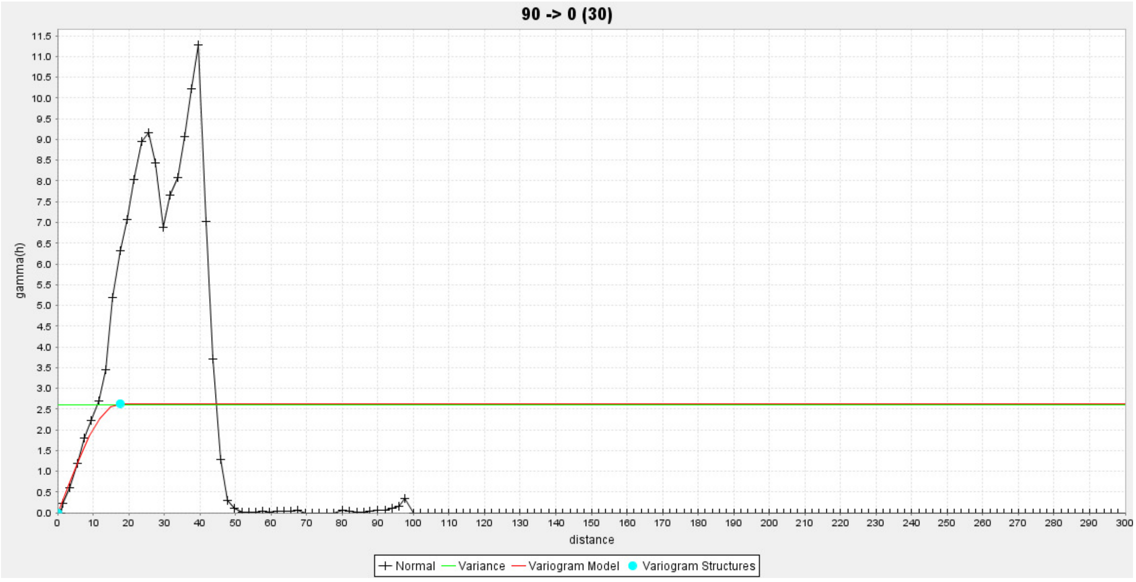
CaO horizontal variogram



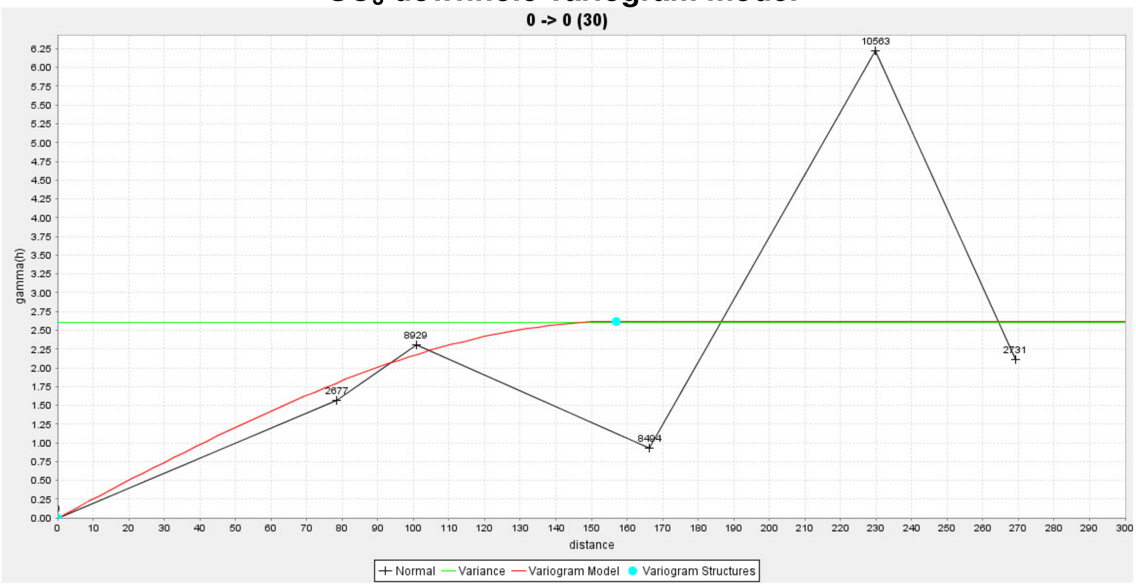
P_2O_5 downhole variogram model



P_2O_5 horizontal variogram model



SO_3 downhole variogram model



SO_3 horizontal variogram model

Appendix 4

JORC Consent Form

Tim Callaghan – Resource and Exploration Geology
3 Main Rd Penguin 7318 ph. 0428 888 896 email: timcallaghan@netspace.net.au

Competent Person's Consent Statement
Pursuant to the requirements of ASX listing rule 5.6 and clause 8 of 2004 JORC code
("Consent statement")

Report name: KARA NO2 NORTH MINERAL RESOURCE ESTIMATE
Dated: MAY 2011

I, Timothy John Callaghan confirm that:

- I have read and understood the requirements of the 2004 edition of the Australasian Code for Reporting of Exploration Results, Minerals Resources and Ore Reserves ("2004 JORC Code").
- I am a competent person as defined by the 2004 JORC Code, having five years experience which is relevant to the style of mineralization and type of deposit described in the report, and to the activity for which I am accepting responsibility.
- I am a member or fellow of the *Australasian Institute of Mining and Metallurgy* or the *Australian Institute of Geoscientists* or a *'Recognised Overseas Professional Organisation'* ('ROPO') included in a list promulgated by the ASX from time to time.
- I have reviewed the report to which this consent statement applies.
- I am a full time employee of OR I am a consultant working for ***Tim Callaghan – Resource and Exploration Geology*** and have been engaged by ***Forward Mining Ltd*** to prepare the report for ***Kara No2 North Resource Estimation*** for the period ended ***May 2011***.

I verify that the Report is based on and fairly and accurately reflects in the form and context in which it appears the information in my supporting documentation relating to Ore Resources.

I consent to the release of the report and this consent statement by the directors of:
Forward Mining Ltd.

Signature of Competent Person: T. Callaghan

Date: 5th May 2011

Professional Membership: ***Australian Institute of Mining and Metallurgy***

Membership Number: ***222210***

Signature of Witness: [signature]

Appendix 5

Bulk Density Data

First pass				Second Pass			
Samp. ID	**Dry Weight 1**	**Wet Weight 1**	**Density**	**Samp. ID**	**Dry Weight 1**	**Wet Weight 1**	**Density**
KND002 43.3-44	348.0	253.2	3.67	KND002 43.3-44	269.8	197.5	3.73
KND002 44-45	462.7	364.6	4.72	KND002 44-45	338.3	261.8	4.42
KND002 45-46	397.3	307.7	4.43	KND002 45-46	305.9	229.9	4.03
KND002 46-47	212.3	157.1	3.85	KND002 46-47	187.2	134.7	3.57
KND002 47-48	183.9	138.4	4.04	KND002 47-48	152.9	118.8	4.48
KND002 48-49	272.9	210.9	4.40	KND002 48-49	237.7	182.4	4.30
KND002 49-50	242.2	186.1	4.32	KND002 49-50	158.8	122.4	4.36
KND002 50-51	381.0	288.8	4.13	KND002 50-51	369.0	283.5	4.32
KND002 51-52	341.5	267.0	4.58	KND002 51-52	337.3	264.3	4.62
KND002 52-53	223.3	172.1	4.36	KND002 52-53	163.1	119.7	3.76
KND002 53-54	310.6	225.9	3.67	KND002 53-54	188.3	139.9	3.89
KND002 54-55	228.2	173.4	4.16	KND002 54-55	125.2	93.9	4.00
KND002 55-56	278.2	209.4	4.04	KND002 55-56	147.9	109.6	3.86
KND003 38.6-39.6	174.1	127.1	3.70	KND003 38.6-39.6	166.4	120.8	3.65
KND003 39.6-40.6	207.2	150.1	3.63	KND003 39.6-40.6	206.1	149.9	3.67
KND003 40.6-41.6	271.4	211.5	4.53	KND003 40.6-41.6	236.7	167.4	3.42
KND003 41.6-42.6	295.2	219.5	3.90	KND003 41.6-42.6	170.9	118.2	3.24
KND003 42.6-43.6	164.0	115.4	3.37	KND003 42.6-43.6	144.0	97.2	3.08
KND003 43.6-44.6	209.2	155.5	3.90	KND003 43.6-44.6	204.6	152.6	3.93
KND003 44.6-45.6	200.9	145.2	3.61	KND003 44.6-45.6	181.6	135.7	3.96
KND003 45.6-46.6	213.8	162.2	4.14	KND003 45.6-46.6	152.9	115.2	4.06
KND003 46.6-47.6	267.8	198.2	3.85	KND003 46.6-47.6	150.5	108.7	3.60
KND004 37-38	181.4	128.9	3.46	KND004 37-38	175.4	126.2	3.57
KND004 38-39	207.8	149.5	3.56	KND004 38-39	173.7	126.9	3.71
KND004 39-40.2	175.2	121.4	3.26	KND004 39-40.2	124.3	81.9	2.93
KND004 40.2-41.2	211.8	149.3	3.39	KND004 40.2-41.2	141.6	101.3	3.51
KND004 41.2-42.2	191.8	135.1	3.38	KND004 41.2-42.2	185.9	133.9	3.58
KND004 42.2-43.5	213.6	153.4	3.55	KND004 42.2-43.5	110.0	80.1	3.68
KND004 43.5-44.5	280.0	201.8	3.58	KND004 43.5-44.5	222.5	164.7	3.85
KND004 44.5-45.5	320.4	232.1	3.63	KND004 44.5-45.5	283.0	207.6	3.75
KND004 45.5-46.5	233.1	169.4	3.66	KND004 45.5-46.5	103.1	76.0	3.80
KND004 46.5-47.5	200.9	150.0	3.95	KND004 46.5-47.5	105.7	78.1	3.83
KND004 47.5-48.5	191.7	144.7	4.08	KND004 47.5-48.5	126.5	95.1	4.03
KND004 48.5-49.5	207.0	157.3	4.16	KND004 48.5-49.5	163.1	120.4	3.82
KND004 49.5-50.5	308.0	227.1	3.81	KND004 49.5-50.5	304.8	226.1	3.87
KND004 50.5-51.5	270.3	198.2	3.75	KND004 50.5-51.5	226.1	168.0	3.89
KND004 51.5-52.5	213.1	159.1	3.95	KND004 51.5-52.5	185.6	137.6	3.87
KND004 52.5-53.5	236.4	177.5	4.01	KND004 52.5-53.5	194.6	152.4	4.61
KND004 53.5-54.5	324.2	255.0	4.68	KND004 53.5-54.5	104.5	81.7	4.58
KND004 54.5-55.5	123.8	90.4	3.71	KND004 54.5-55.5	77.4	57.6	3.91
KND004 55.5-56	218.8	171.4	4.62	KND004 55.5-56	113.2	86.3	4.21
KND004 56-57	121.8	92.8	4.20	KND004 56-57	110.2	86.6	4.67
KND004 57-58	172.6	134.9	4.58	KND004 57-58	167.8	132.9	4.81
KND004 58-59	131.3	101.6	4.42	KND004 58-59	91.4	70.9	4.46
KND004 59-60	182.4	142.3	4.55	KND004 59-60	155.9	123.9	4.87

Appendix 6

Independent Laboratory Checks


Independent Lab Test SGS BRL
y = 0.9784x
SGS Fe %
BRL Fe %
0
10
20
30
40
50
60